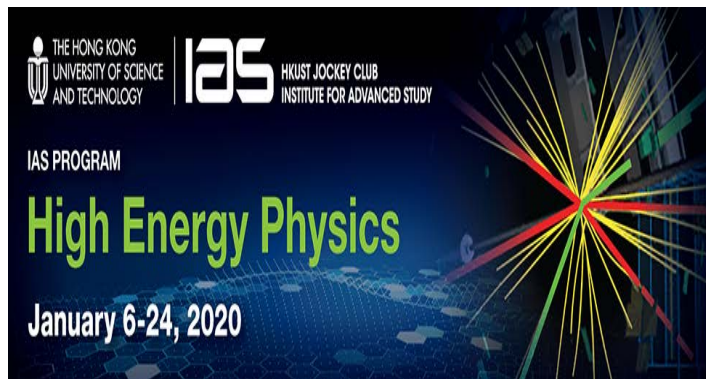


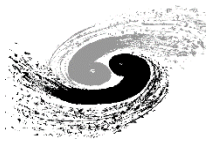
CEPC Linac Injector R&D

Jingru Zhang

On behalf of CEPC linac team

Institute of High Energy Physics, CAS





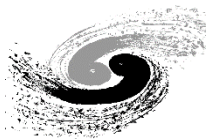
Outline

1 Linac baseline design

2 Linac alternatives

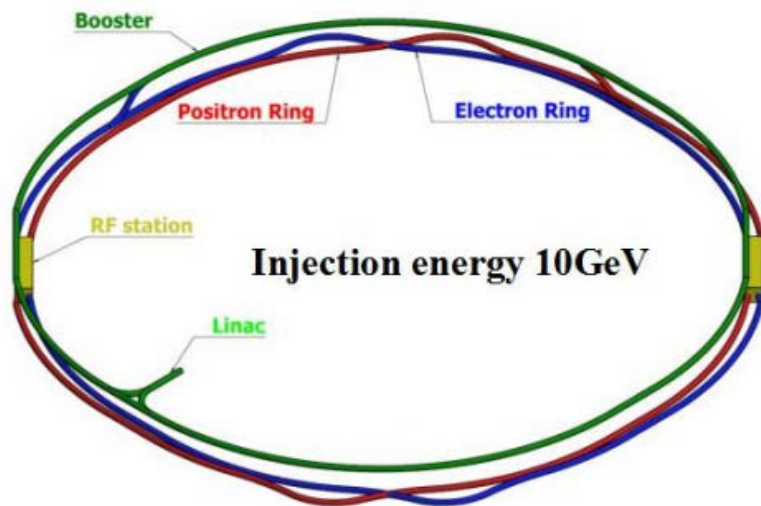
3 R&D activities

4 Summary

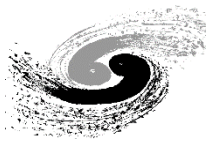


Linac baseline design

- CEPC consists of Linac, Booster and Collider
 - The energy electron and positron of the Collider is 120 GeV.
 - The booster and collider circumference is about 100 km



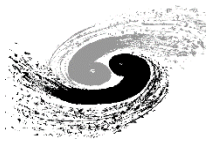
- The linac injector provides 10 GeV electron and positron beam to the Booster
- The total length of the linac is about 1.2 km



Linac baseline design

- The requirements of the booster to the linac

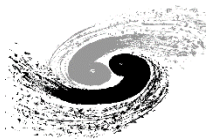
Parameter	Symbol	Unit	Value
e^- / e^+ beam energy	E_{e^-} / E_{e^+}	GeV	10
Repetition rate	f_{rep}	Hz	100
Bunch numbers per pulse			1
e^- / e^+ bunch population	N_{e^-} / N_{e^+}		$>9.4 \times 10^9$
		nC	>1.5
Energy spread (e^- / e^+)	σ_E		$<2 \times 10^{-3}$
Emittance (e^- / e^+)	ε_r	nm	<40



Linac baseline design

• Linac design goals

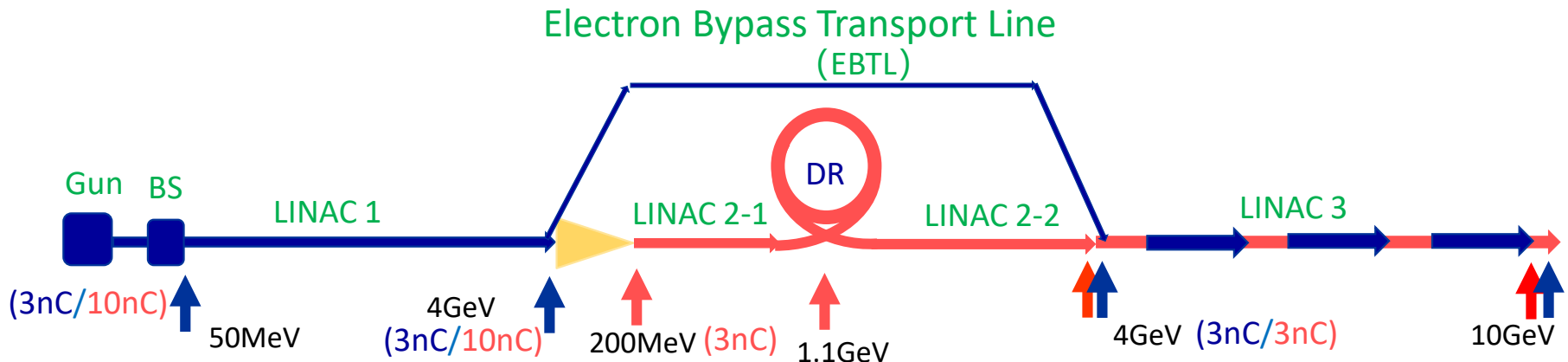
- Meet the requirements of Booster injector
- Top-up injection can be implemented
- High availability and reliability
 - ◆ About 15% backups for linac RF units
- More potential
 - ◆ Have potential to provide electron/positron beam with bunch charge large than 3 nC
 - ◆ Lower emittance with more cycles in Damping Ring

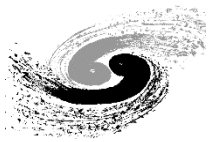


Linac baseline design

• Layout of the linac

- Electron linac (Pre-injector+Linac 1+EBTL+Linac 3)
- Positron linac (Pre-injector+Linac 1+PS+Linac 2-1+DR+Linac 2-2+Linac 3)





Outline

1 Linac design

2 Linac alternatives

3 R&D activities

4 Summary



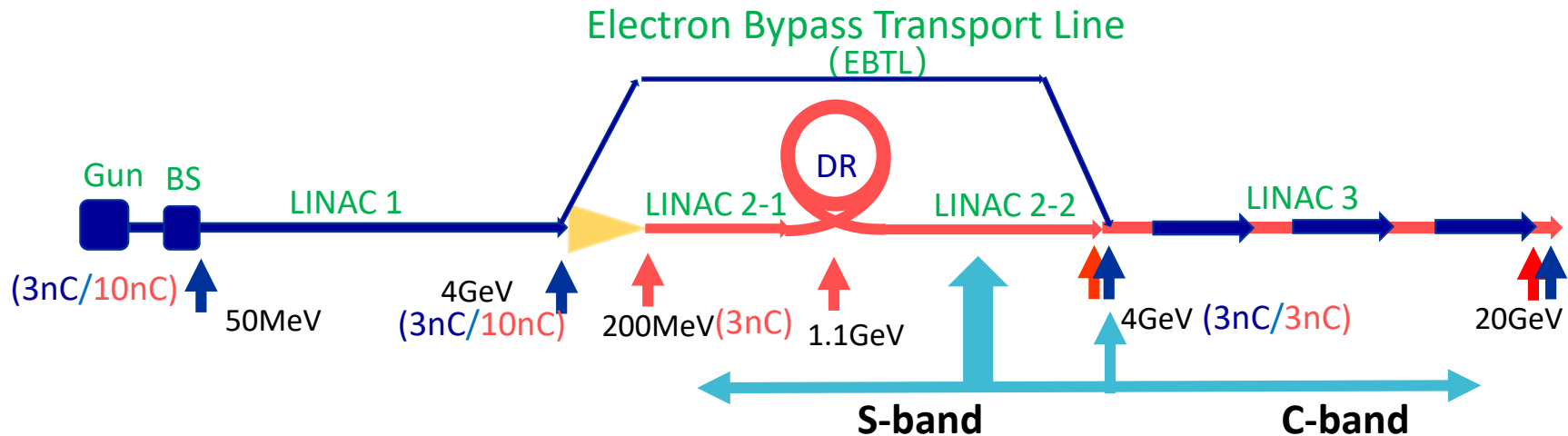
Linac alternative (1)

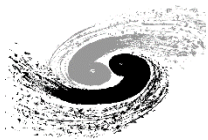
- 20 GeV linac

- Reduce the difficulty of the Booster design
- Reduce the technical risk of low magnetic field magnets of the Booster

- S-band+C-band RF system

- C-band start energy: 4GeV
- If the DR can provide lower emittance, the C-band start energy can move forward





Linac alternative (1)

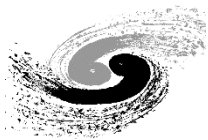
- 20GeV linac (S-band + C-band)
 - The gradient of C-band structure is 45 MV/m
 - The total length is 1.4 km, 200 m longer than the baseline design

The main parameters of the linac exit

Parameter	Unit	S-band	C-band
Frequency	MHz	2860	5720
Length	m	3.1	1.8
Cavity mode		$2\pi/3$	$3\pi/4$
Aperture diameter (mm)	mm	20~24	11.8~16
Gradient	MV/m	21	45

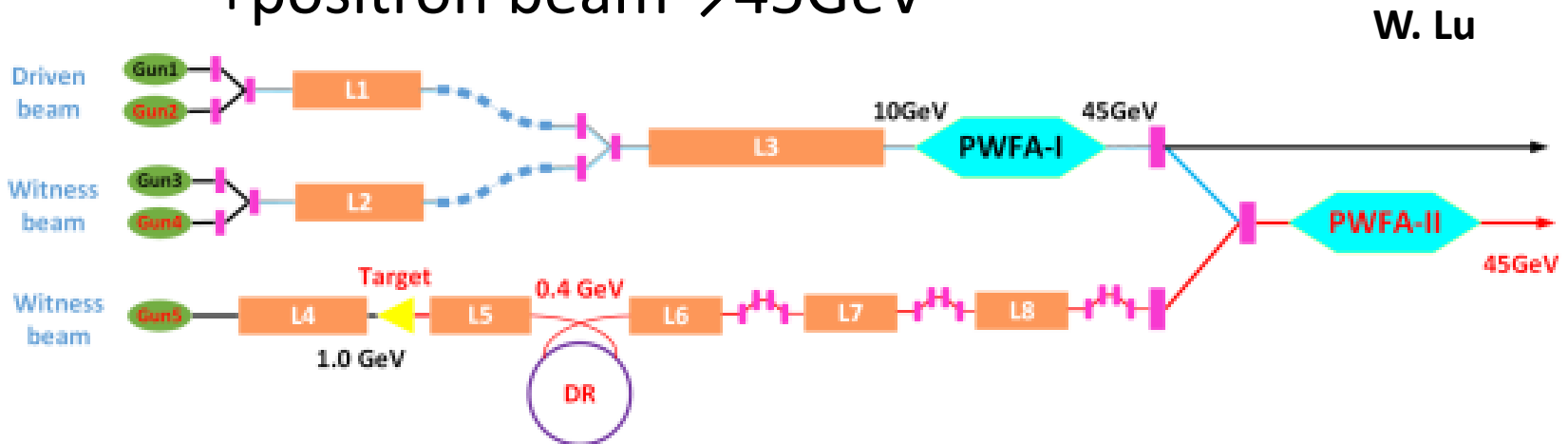
Parameter	Symbol	Unit	Baseline	Alternative
e^-/e^+ beam energy	E_{e^-}/E_{e^+}	GeV	10	20
Repetition rate	f_{rep}	Hz	100	100
Bunches/pulse			1	1
e^-/e^+ bunch population	N_{e^-}/N_{e^+}		$>9.4 \times 10^9$	$>9.4 \times 10^9$
		nC	>1.5 (3)	>1.5 (3)
Energy spread (e^-/e^+)	σ_E		$<2 \times 10^{-3}$	$<2 \times 10^{-3}$
Emittance (e^-/e^+) Req.	ϵ_r	nm	< 40	< 20
Length	L	m	1200	1400

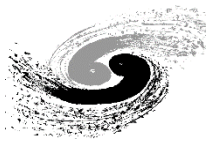
The main parameters of the C-band structure



Linac alternative (2)

- Plasma wakefield accelerator (45GeV linac)
 - Electron linac
 - ◆ 10GeV driver linac+Plasma linac→45GeV
 - ◆ The Plasma linac is like a power transformer
 - Positron linac
 - ◆ 45GeV or 30GeV driver electron beam +positron beam→45GeV





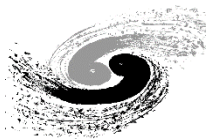
Outline

1 Linac design

2 Linac alternatives

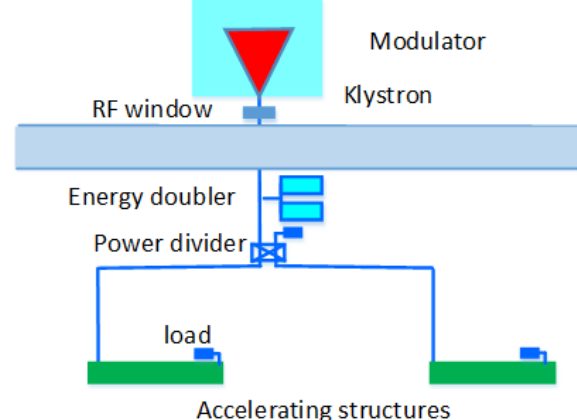
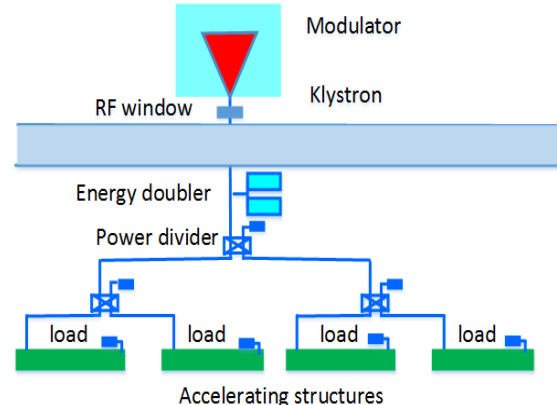
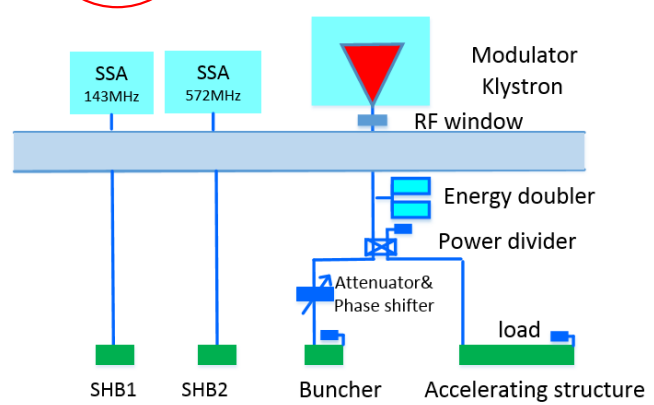
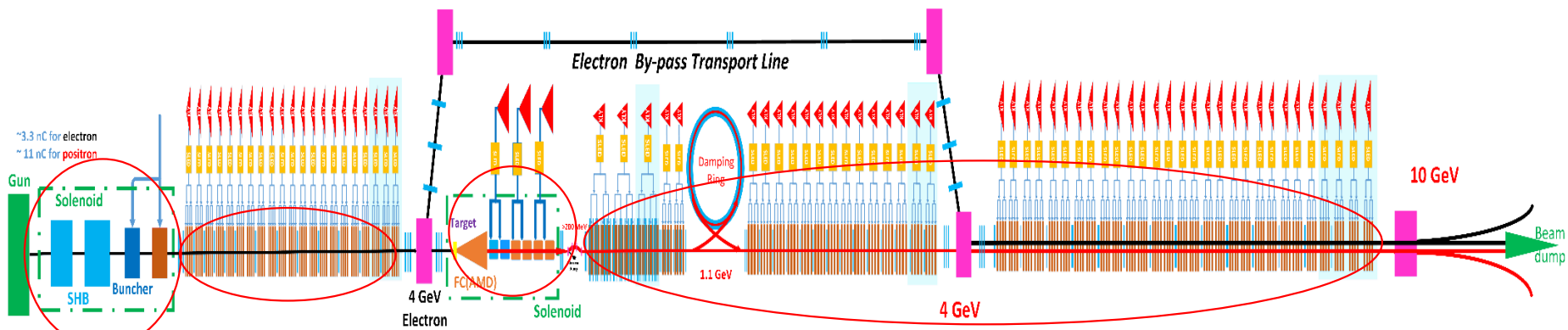
3 R&D activities

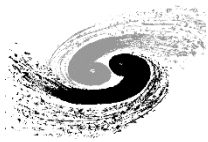
4 Summary



R&D activities

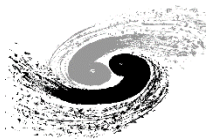
- RF distribution of the linac
 - S-band accelerating structures
 - 80MW klystron





R&D activities

- Key RF technologies of linac baseline
 - Electron gun (1)
 - SHBs (2)
 - Buncher (1)
 - **S-band accelerating structure (277)**
 - **Pulse compressor (72)**
 - **Positron source (1)**
 - Big hole accelerating structure (6)
 - DR 650MHz RF cavity (2)
 - LLRF (75)
 - Phase reference line (1)
 -

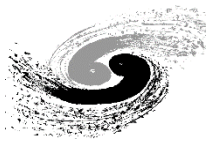


Accelerating structure

- S-band accelerating structure design

- Motivation: It is more than 280 S-band (2860MHz) accelerating structures
- Goal: Accelerating gradient more than 30 MV/m @1 μ S

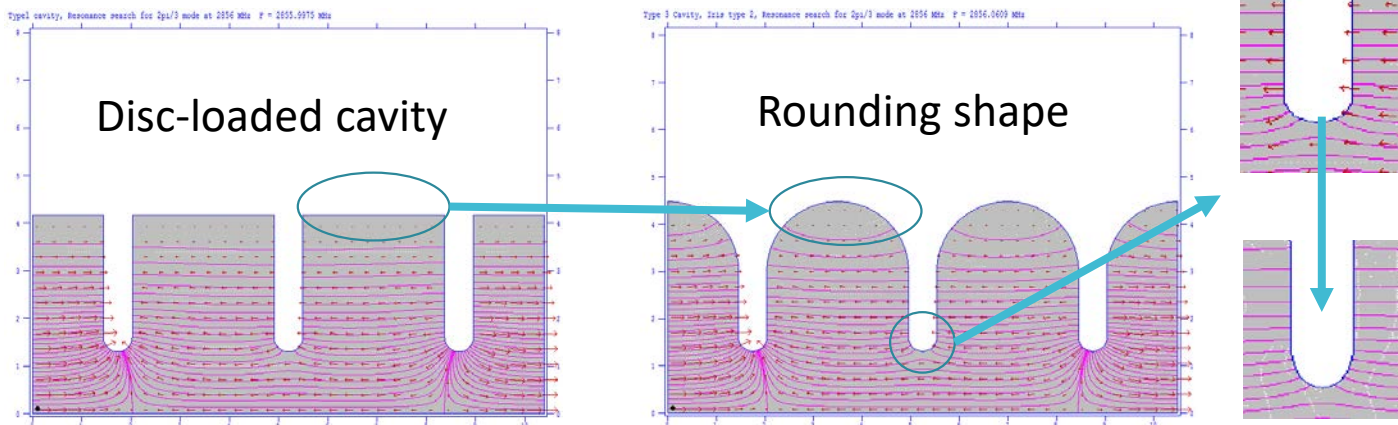


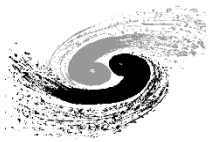


Accelerating structure

● Cavity shape optimization

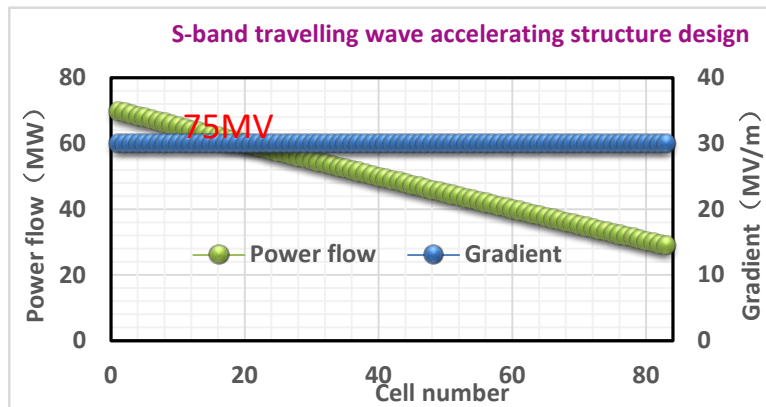
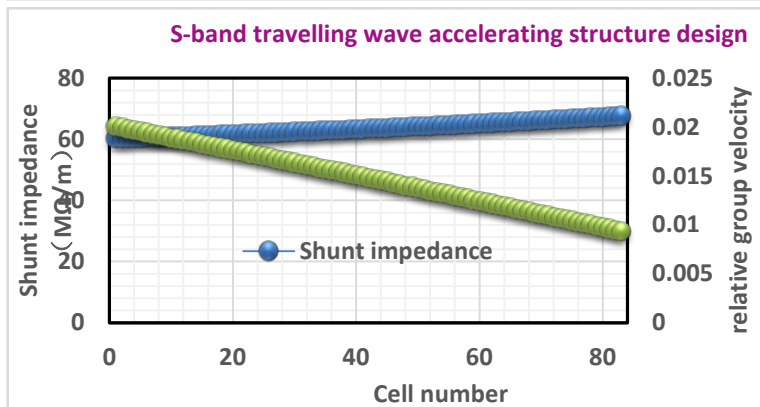
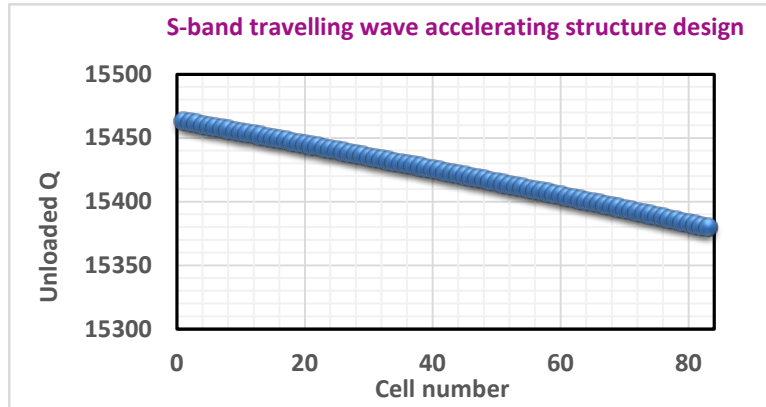
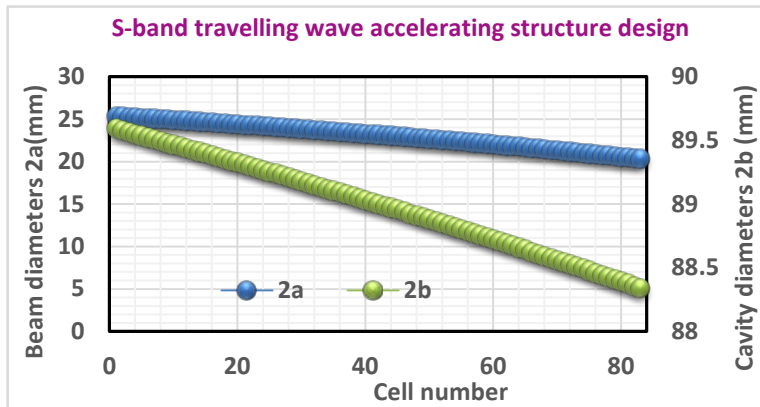
- Superfish is used to optimize the single cell
- Rounding the cell improves the quality factor by >12% and reduces the wall power consumption. At the same time, the shunt impedance increases by ~10.9%
- Irises with elliptical shape ($r_2/r_1=1.8$) can reduce the peak surface field by 13%

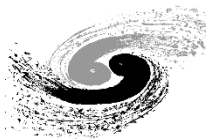




Accelerating structure

- The total number of cells of the tube is 84
- The average Q value is about 15400
- The input power is 75MW , the target gradient will reached





Accelerating structure

- Factors to limit the gradient (cavity):

- Peak surface electric field (E_{peak})

- ◆ $E_{\text{peak}} < 160 \text{ MV/m}$ at S-band

- Peak surface magnetic field (H_{peak})

- ◆ Pulsed heating effect will cause the temperature rise at

the coupler window. $\Delta T = \frac{|H_{||}|^2 \sqrt{t_p}}{\sigma \delta \sqrt{\pi \rho c k}}$, for S-band $\Delta T < 50^\circ\text{C}$

is safe

- Modified Poynting vector (S_c),

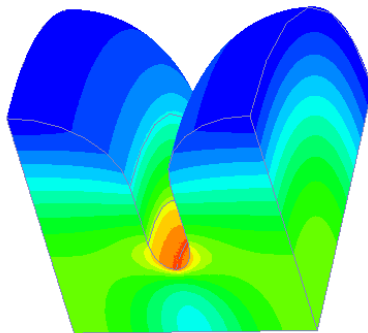
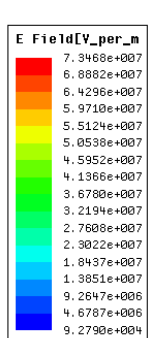
- ◆ $S_c = \text{Re}\{\bar{s}\} + \frac{\text{Im}\{\bar{s}\}}{6}$, $\frac{S_c^{15} t_p^5}{BDR} = \text{const.}$ If the beam break down rate is $1 \cdot 10^{-6} \text{ bpp/m}$, the safe value for $1 \mu\text{s}$ pulse length is 2.3 MW/mm^2

- Pulse length ($1 \mu\text{s}$)



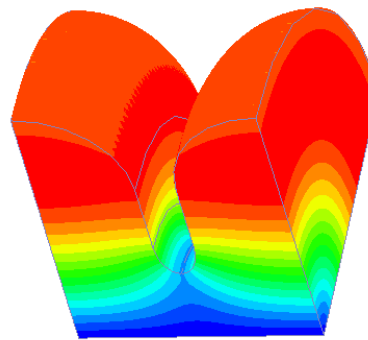
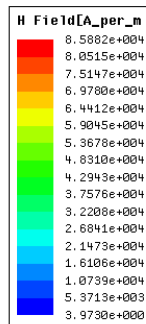
Accelerating structure

- Factors to limit the gradient (cavity):
 - 3D program HFSS is used to confirm the design
 - The 1st cell adjacent the input coupler is simulated for $P_{in}=75$ MW
 - The values are safe. Both E_{peak} and Sc locates at the iris area



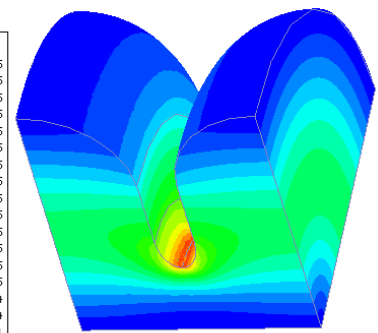
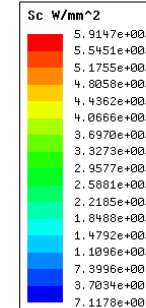
$E_{peak}=73$ MV/m.

Surface electric field



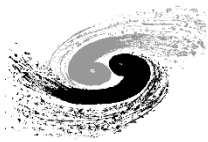
$H_{peak}=86$ kA/m.

Surface magnetic field



$Sc_{max}=0.59$ MW/mm².

Modified Poynting vector



Accelerating structure

- The main parameters of the whole structure
 - The filling time is 784 ns
 - The total attenuation is 0.46 Np

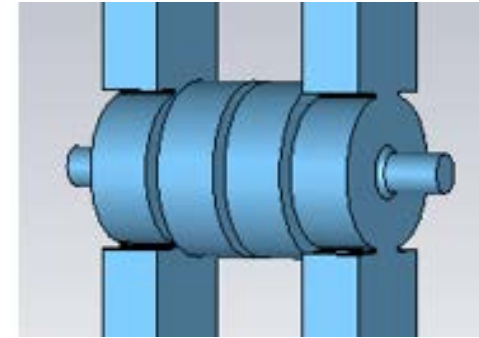
Parameters	Values	Unit
No. of Cells	$84+2*0.5$	-
Phase advance	$2\pi/3$	rad
Total length	3.1	m
Length of cell (d)	34.988	mm
Disk thickness (t)	5.5	mm
Shunt impedance (R_s)	60.3~67.8	M Ω /m
Quality factor	15465~15373	-
Group velocity: V_g/c (%)	2% ~ 0.94%	-
Filling time (t_f)	784	ns
Attenuation factor (τ)	0.46	Np



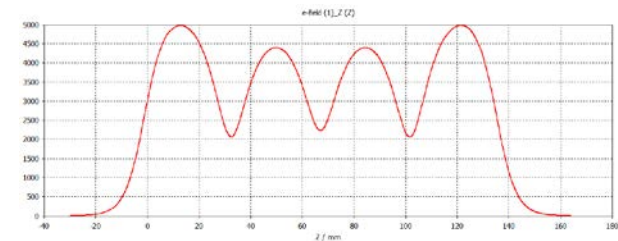
Accelerating structure

• Coupler design

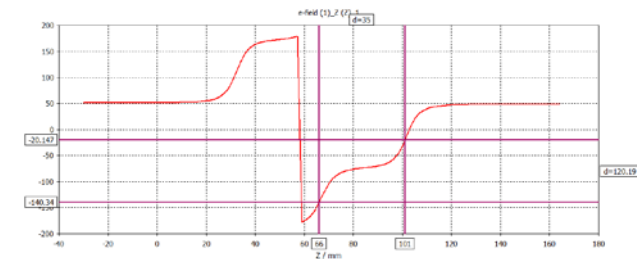
- The asymmetry of the coupling cavity will cause emittance growth
- The shape of the coupling cavity is racetrack dual-feed type
- Kyhl method is used to match the coupler



The calculation model



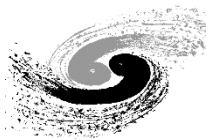
The *distribution of the electric field on axis*



Phase advance per cell

$$\varepsilon_{n-final} = \sqrt{\varepsilon_{n-initial}^2 + \sigma_x^2 \left(\frac{\sigma \Delta p_x}{mc} \right)^2}$$

$$\Delta p_x = -\frac{e \Delta z E_0}{2 \omega a} \left[\Delta \theta * \sin \varphi - \frac{\Delta E}{E_0} \cos \varphi \right]$$



Accelerating structure

• Factors to limit the gradient (coupler):

- To reduce the pulsed heating, the coupler window edge is rounded.

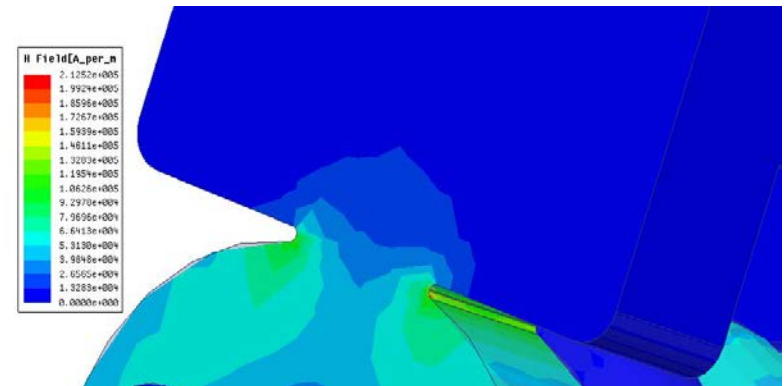
- For S-band copper: $\Delta T[^{\circ}\text{C}] = 127 |H_{||} [\text{MA}/\text{m}]|^2 \sqrt{f \cdot [\text{GHz}] \cdot t_p [\mu\text{S}]}$

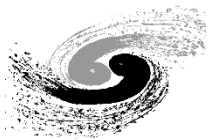
- For 75 MW input power, the maximum value of the peak surface magnetic field is $2.1 \cdot 10^5$ A/m. for $1 \mu\text{S}$ pulse length, $\Delta T = 9.4^{\circ}\text{C}$.

$$\Delta T = \frac{|H_{||}|^2 \sqrt{t_p}}{\sigma \delta \sqrt{\pi \rho c k}}$$

Labels and their corresponding variables in the equation:

- Magnetic field → $|H_{||}|$
- RF Pulse length → $\sqrt{t_p}$
- Electric conductivity → σ
- Skin depth → δ
- Material density → ρ
- Specific heat → c
- Thermal conductivity → k

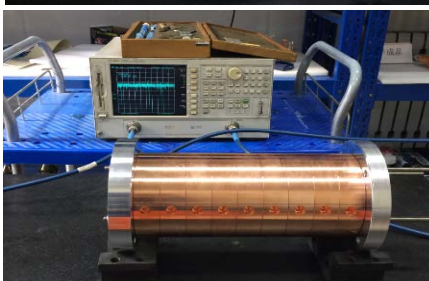


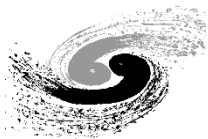


Accelerating structure

● Mechanical design

- Inner water-cooling has been adopted. 8 pipes are around the cavity.
- Compact coupler arrangements. The splitter is milling together with the coupling cavity.
- Two tuners are outside the cavity.

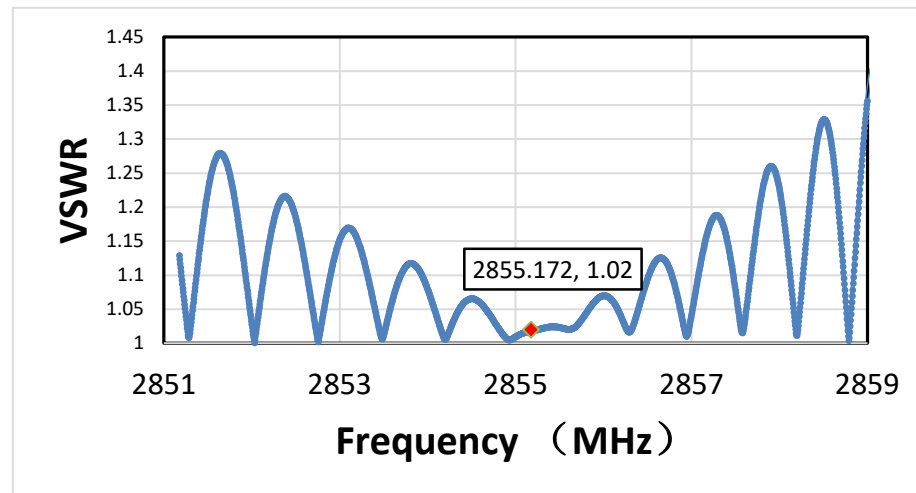
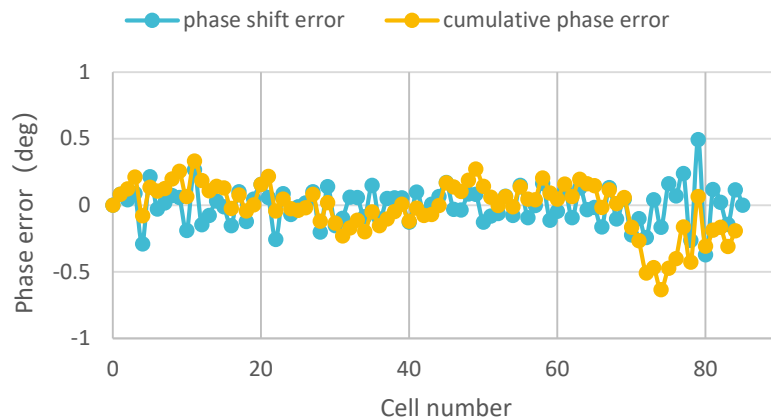


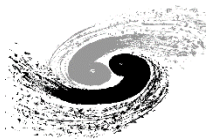


Accelerating structure

● Cold test result

- The phase shift and the cumulative phase shift are less than 1 deg
- The VSWR is 1.02 at working frequency





Accelerating structure

• High power test

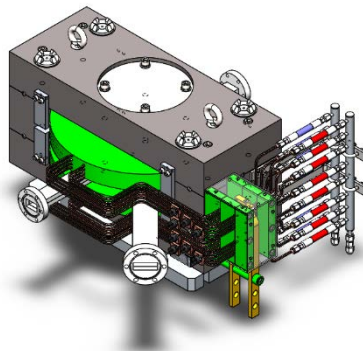
- Two faraday cups are in upstream and downstream of the structure to detect dark current respectively
- The high power test gradient has been more than 25 MV/m
- Higher gradient practice is in progress



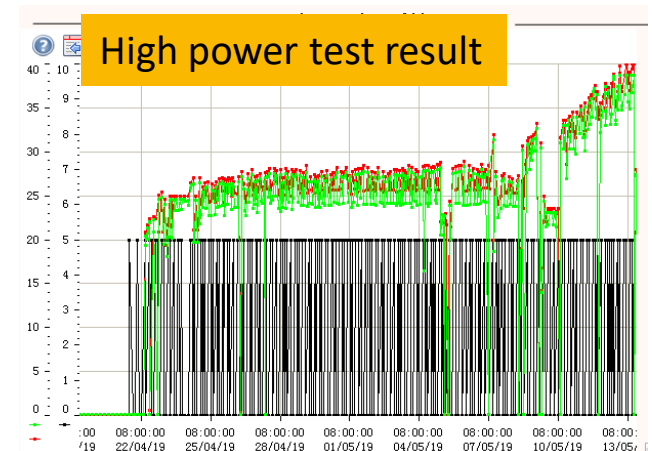
Modulator and klystron

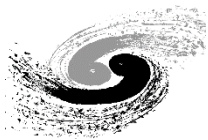


High power test bench



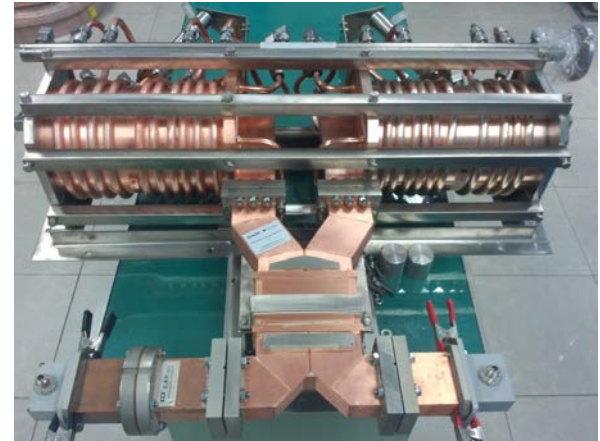
Analyzing Magnet



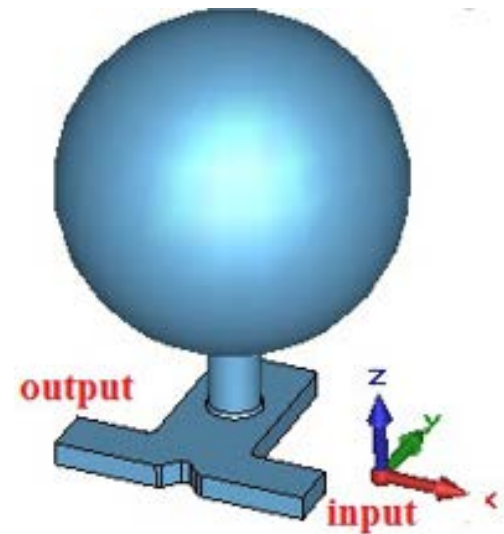
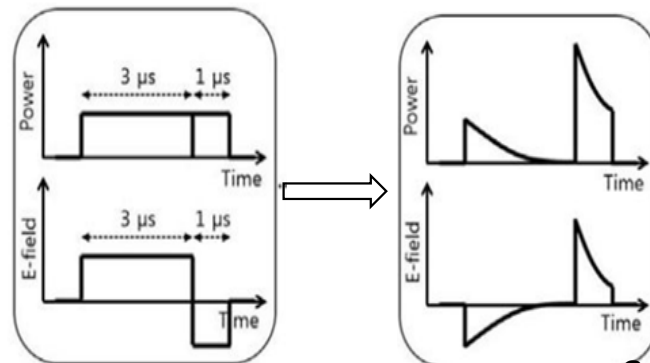
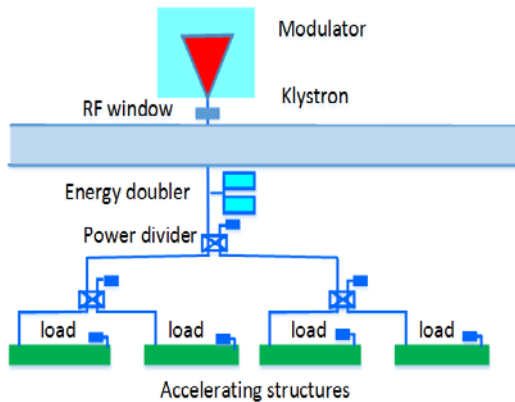


Pulse compressor

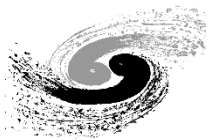
- It is used to improve the peak power from the klystron and saving cost
 - The input power is 80 MW
 - The pulse width has been compressed from $4\mu\text{s} \rightarrow 1\mu\text{s}$
- The traditional pulse compressor is two cavities SLED type
- The new one is spherical cavity type



SLED

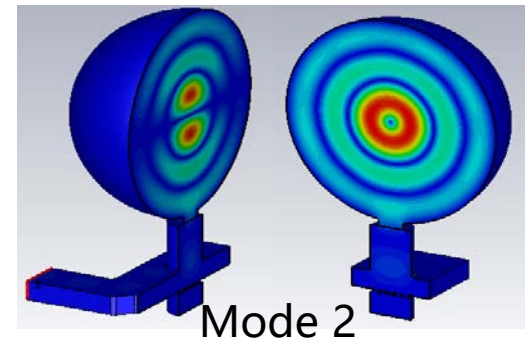
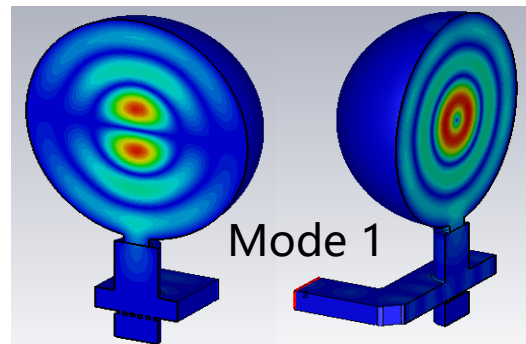
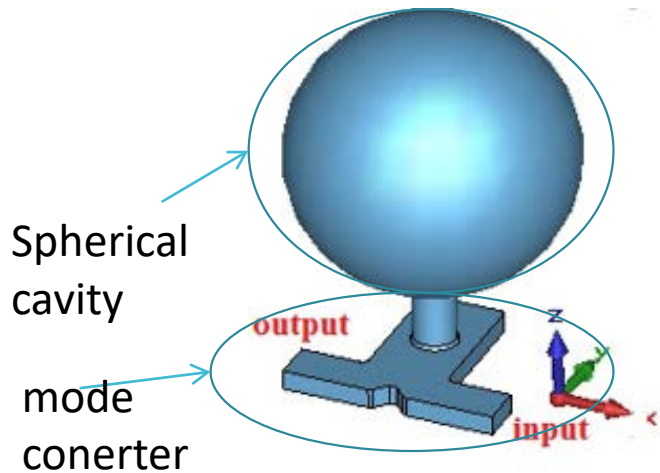


Spherical cavity pulse compressor



Pulse compressor

- The advantage of the spherical cavity pulse compressor
 - Only one cavity is needed, which is more compact, lower processing cost
 - Surface loss is smaller than that of the cylindrical cavity
 - Good in mechanical stability and little in environmental impact
- TE_{113} mode is selected
- Two polarized degeneracy mode are in one cavity
- The structure includes mode converter and spherical cavity



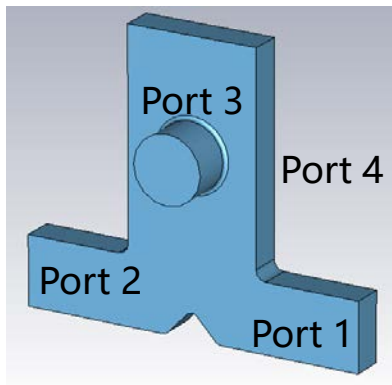
E-field distribution of the polarized degenerated modes



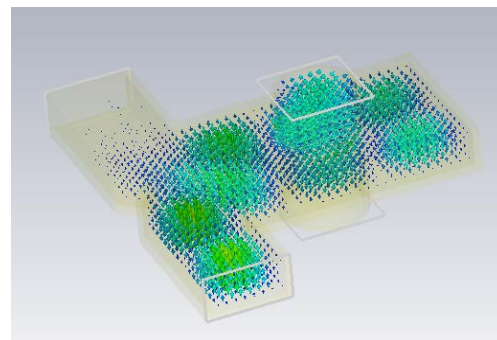
Pulse compressor

• Mode converter

- The TE_{10} mode input from Port 1 will be converted into two degenerated TE_{11} modes at Port 3
- There are two degenerated TE_{113} modes in the spherical cavity, The phase difference of the two modes is about 90°
- The input port S_{11} is -62.7 dB
- The S_{41} is -71dB and port 4 is for vacuum

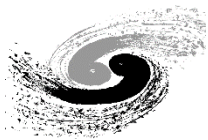


Vacuum model



Electromagnetic field

S_{11} / VSWR	-62.7 dB/1.0016
S_{21}	-42.9 dB
$S_{31}(1)$	-3.02 dB
$S_{31}(2)$	-3.02 dB
Phase difference of two modes	89.89°
$S_{41}(1)$	-70.9 dB
$S_{41}(2)$	-71.0 dB



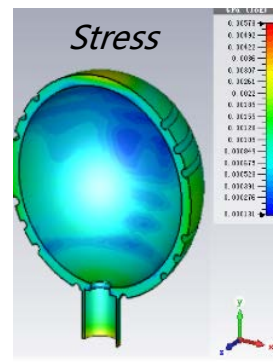
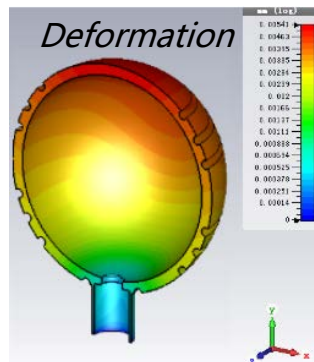
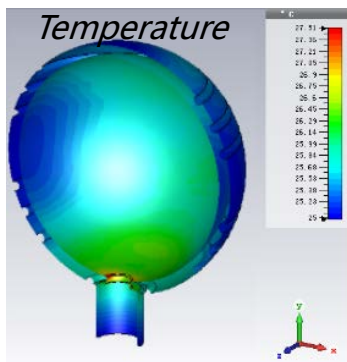
Pulse compressor

• Thermal stress analysis

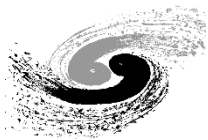
- The maximal temperature rise is on the coupling hole of 2.5 °C (the water cooling flow set as 50 L/min)
- The frequency tunable range of ± 1 MHz is enough for all the frequency shift resulted from the input power, vacuum pumping, air pressure, etc.

CEPC parameter

Parameter	Value
SLED water temperature	30 °C
Room temperature	25 °C
Filling time	730 ns
Klystron output power	80 MW
Pulse width	4 μ s
Pulse repetition rate	100 Hz



- the water temperature will be used to tune the frequency.
- Accordingly, the water temperature need to be ± 3.6 °C change



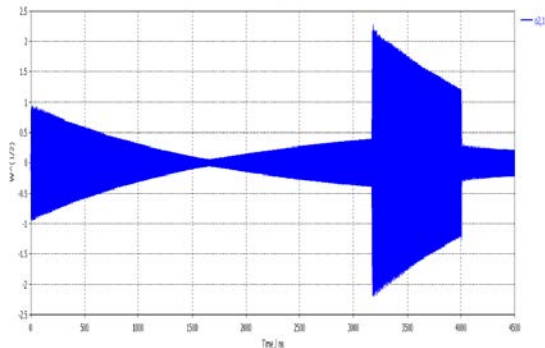
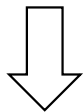
Pulse compressor

• The parameters

- The Q_0 is 146000
- The energy gain factor is ~ 1.6

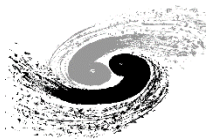
For input signal:

$$f(t) = \begin{cases} \sin(2\pi f_0 t) & 0 \leq t < 3.17 \mu\text{s} \\ \sin(2\pi f_0 t + \pi) & 3.17 \mu\text{s} \leq t < 4 \mu\text{s} \\ 0 & 4 \mu\text{s} \leq t < 4.5 \mu\text{s} \end{cases}$$



Simulated compressed pulse

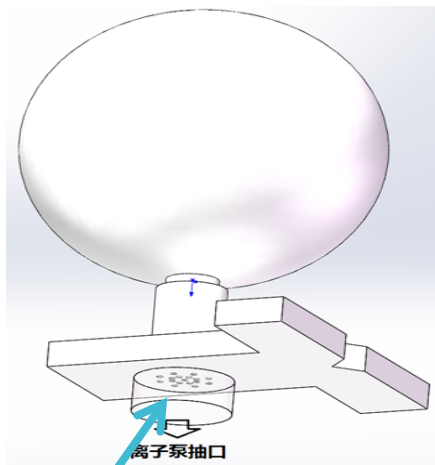
Parameter	value
Frequency	2856 MHz
Mode	TE113
Q_0	~ 146000
VSWR	≤ 1.1
Coupling factor	~ 6.9
Tuning rang	$\geq \pm 1$ MHz
Input power	≥ 80 MW
Repetition fre.	100 Hz
Pulse width	$\sim 4 \mu\text{s}$
Pulse width after compress	$\sim 0.83 \mu\text{s}$
Peak power gain	≥ 7 dB
Energy gain factor	~ 1.6
Working temperature	$30 \pm 0.1^\circ\text{C}$



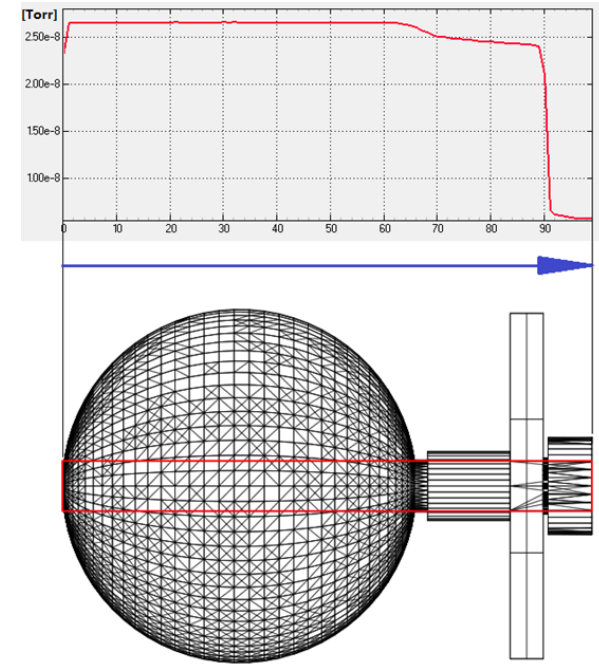
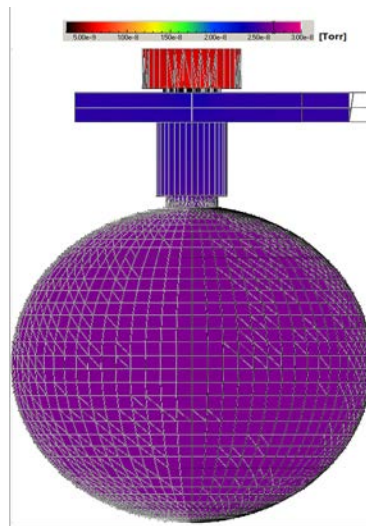
pulse compressor

• Vacuum analysis

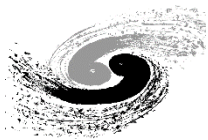
- Pumping speed of ion pump is 100 L/s
- Copper outgassing rate: $1\text{E-}10$ Torr.L/s/cm²
- Pressure distribution: vacuum degree less than $3\text{E-}8$ Torr



Ion pump port



Pressure distribution of longitudinal section



Positron Source

- Layout of positron source

- ◆ Target (Conventional)

- ✓ tungsten@15 mm
- ✓ Beam size: 0.5 mm

- ◆ Electron Beam

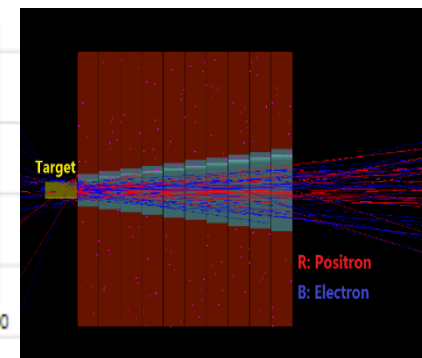
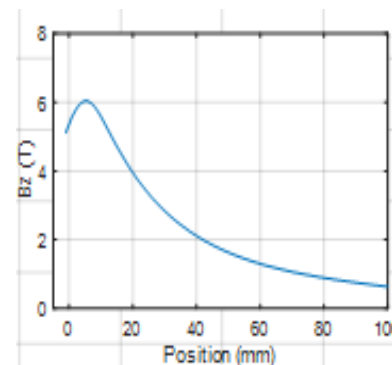
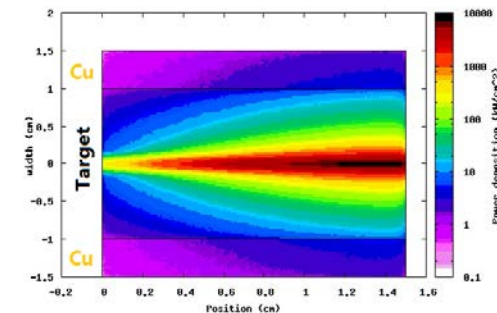
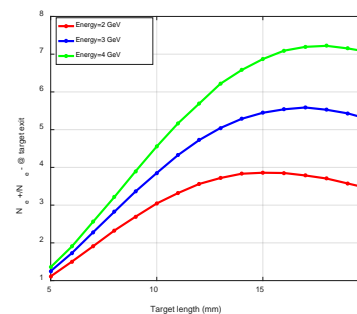
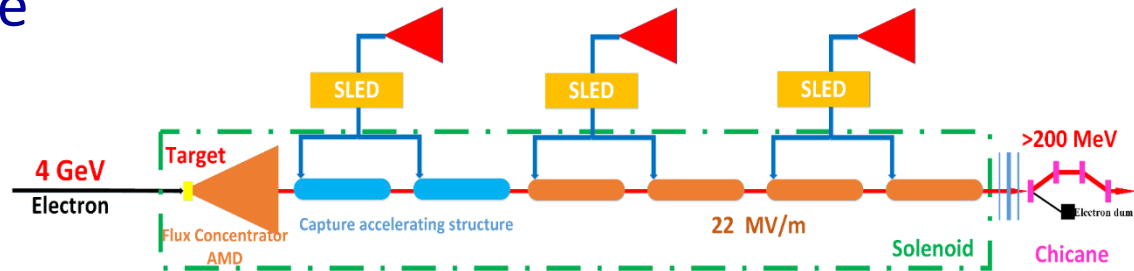
- ✓ 4GeV/10nC/100Hz
- ✓ Beam power 4kW

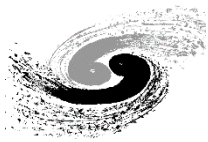
- ◆ Energy deposition

- ✓ 0.784 GeV/e- @ FLUKA
- ✓ 784 W → water cooling

- ◆ AMD (Adiabatic Matching Device)

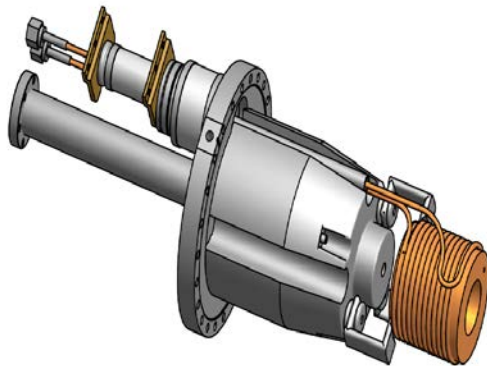
- ✓ Flux Concentrator



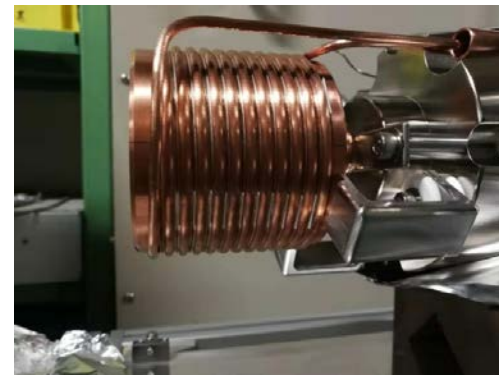


Positron Source

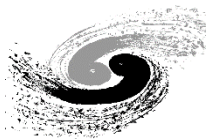
- FLUX concentrator is the important part of the positron source
 - ✓ Length: 100mm
 - ✓ Aperture: 8mm → 26mm
 - ✓ Magnetic field: (5.5T → 0T) + 0.5T
- FLUX concentrator has designed and manufactured



The mechanical design of FLUX concentrator



The finished FLUX concentrator

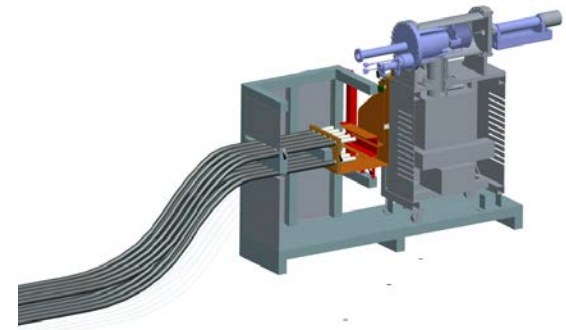


Positron Source

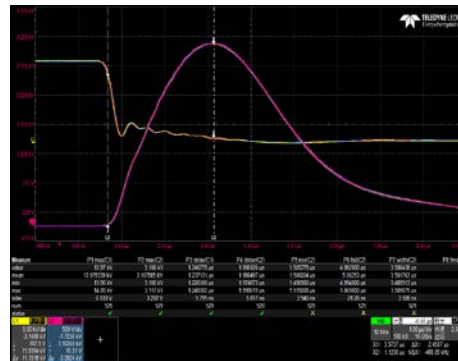
• Solide-state pulsed power generator

- Solid state IGCT discharge switch module is used
- The maximum output value of the solid-state pulsed power generator reached 15.6 kA / 15.1 kV / 5 μ s, the waveform is perfect
- It reached the design value

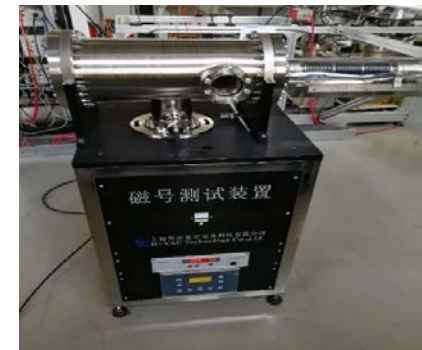
• High power test will begin



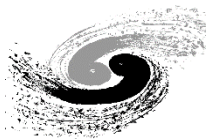
solid-state pulsed power generator



The output waveform of 15 kA



The test bench of the FLUX concentrator

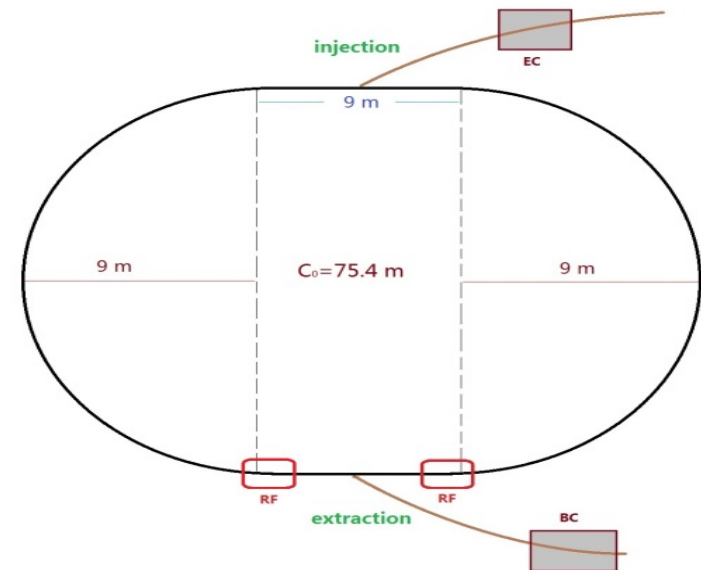
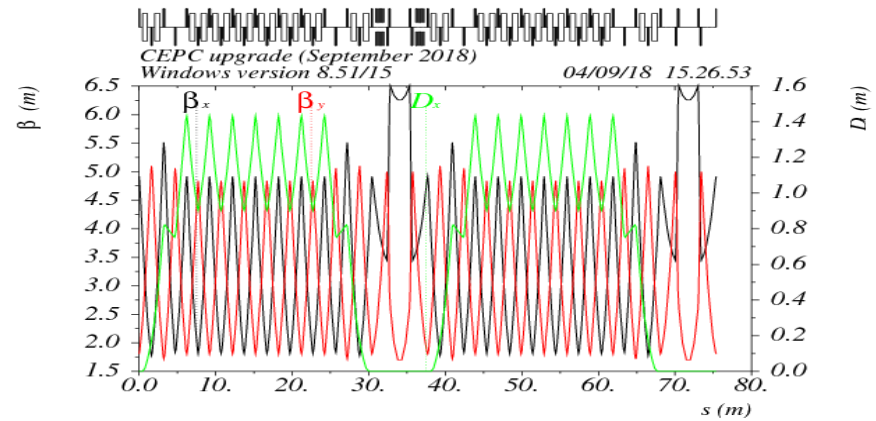


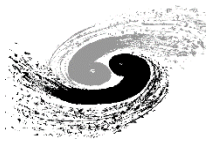
Damping Ring RF cavity

D, Wang

• Damping ring

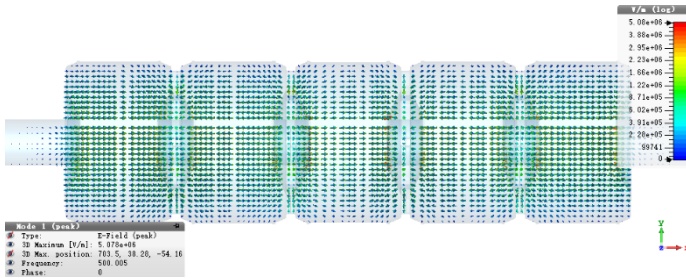
DR V2.0	Unit	Value
Energy	GeV	1.1
Circumference	m	75.4
Storage time	ms	20
Bending radius	M	3.565
Dipole strength B_0	T	1.03
U_0	keV	36.3
Damping time x/y/z	ms	15.2/15.2/7.6
δ_0	%	0.05
ϵ_0	mm.mrad	376.7
$\sigma_{z, inj}$	mm	5.0
Nature σ_z	mm	7.5
ϵ_{inj}	mm.mrad	2500
$\epsilon_{ext x/y}$	mm.mrad	530/180
$\delta_{inj} / \delta_{ext}$	%	0.2/0.05
Energy acceptance by RF	%	1.0
f_{RF}	MHz	650
V_{RF}	MV	2.0



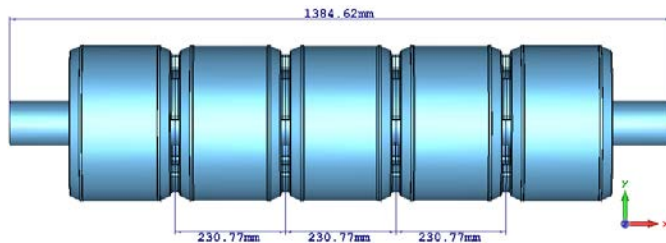


Damping Ring RF cavity

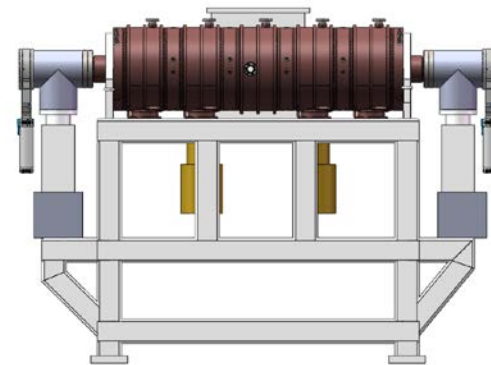
• 650 MHz 5-cell cavity



The electromagnetic distribution

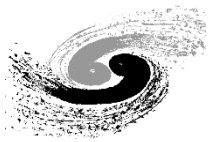


The main dimensions



The mechanical design

	Unit	650 MHz 5-cell
π -mode frequency	MHz	650.0
Unloaded quality factor		26080
$R/(Q \cdot I)$	Ω/m	435
Shunt impedance	$M\Omega$	13.1
Accelerating voltage	MV	1.2
Accelerating gradient	MV/m	1.04
Dissipated cavity power	kW	55



Summary

- The baseline linac design is a 10 GeV S-band linac
- Two alternative schemes of linac have been suggested. One is 20 GeV S&C band linac, the other one is a plasma accelerator
- The key components of the linac baseline are being developed.
 - The accelerating structure is under high power test.
 - The spherical pulse compressor has designed and will be manufactured this years.
 - The FLUX concentrator has also finished and is under high power test.
 - The damping ring RF cavity is simulated.



Thank you for your attention!