

GdBCO Coated Conductor and Magnet Development in SuNAM



Hunju Lee, Jae-Hun Lee, Jaemin Kim, Seung Hyun Moon
SuNAM Co., Ltd.

2018. 2. 18.

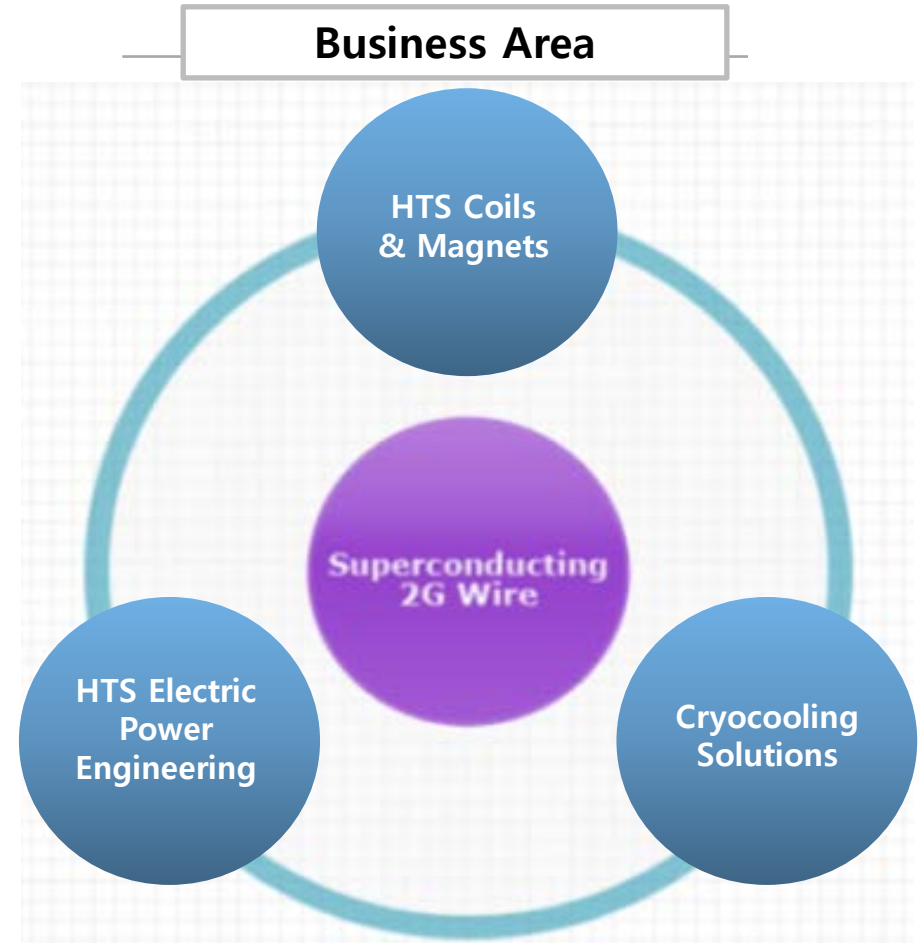
Contents

- **SuNAM's coated conductor; architecture, characteristic, process, quality control**
- **Magnet**
 - **Low field conduction cooled magnet**
 - **Coil for linear synchronous motor**
 - **26 T LHe-cooled magnet**
 - **Conduction-cooled NMR magnet**
 - **18 T magnet for Axion detection**

Company Overview

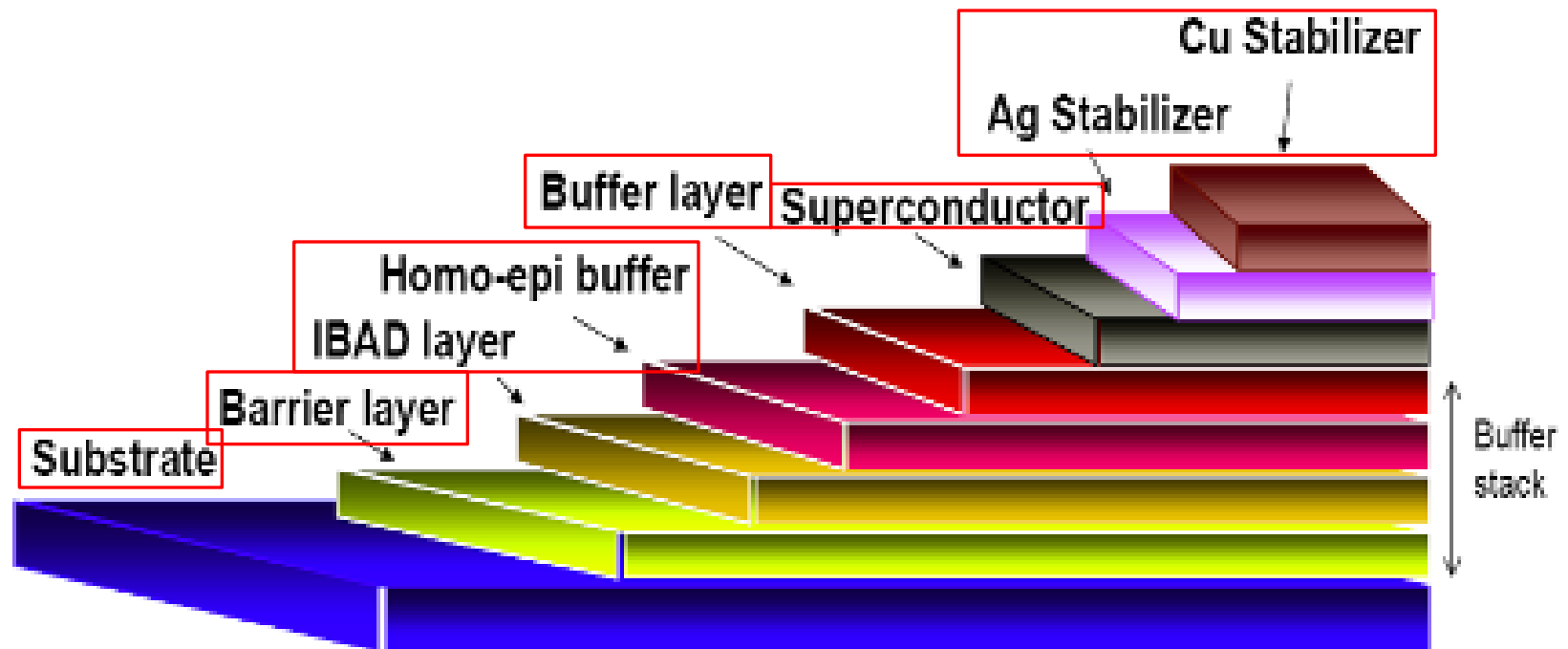
SuNAM : **S**uperconductor, **N**ano & **A**dvanced **M**aterials (서남, 瑞藍)

Establishment	2004. 11. 17., for commercialization of HTS wire
CEO	Seung-Hyun Moon
Registered Capital	~\$6M
No. of Employees	~ 35 (7 Ph.Ds)
H.Q.	Gyeonggi-do, Korea
Current Production Capacity	~ 60 km / month (4 mm > 150 A)
Core Technology	2G HTS manufacturing technology based on RCE-DR process & No-Insulation HTS Magnet



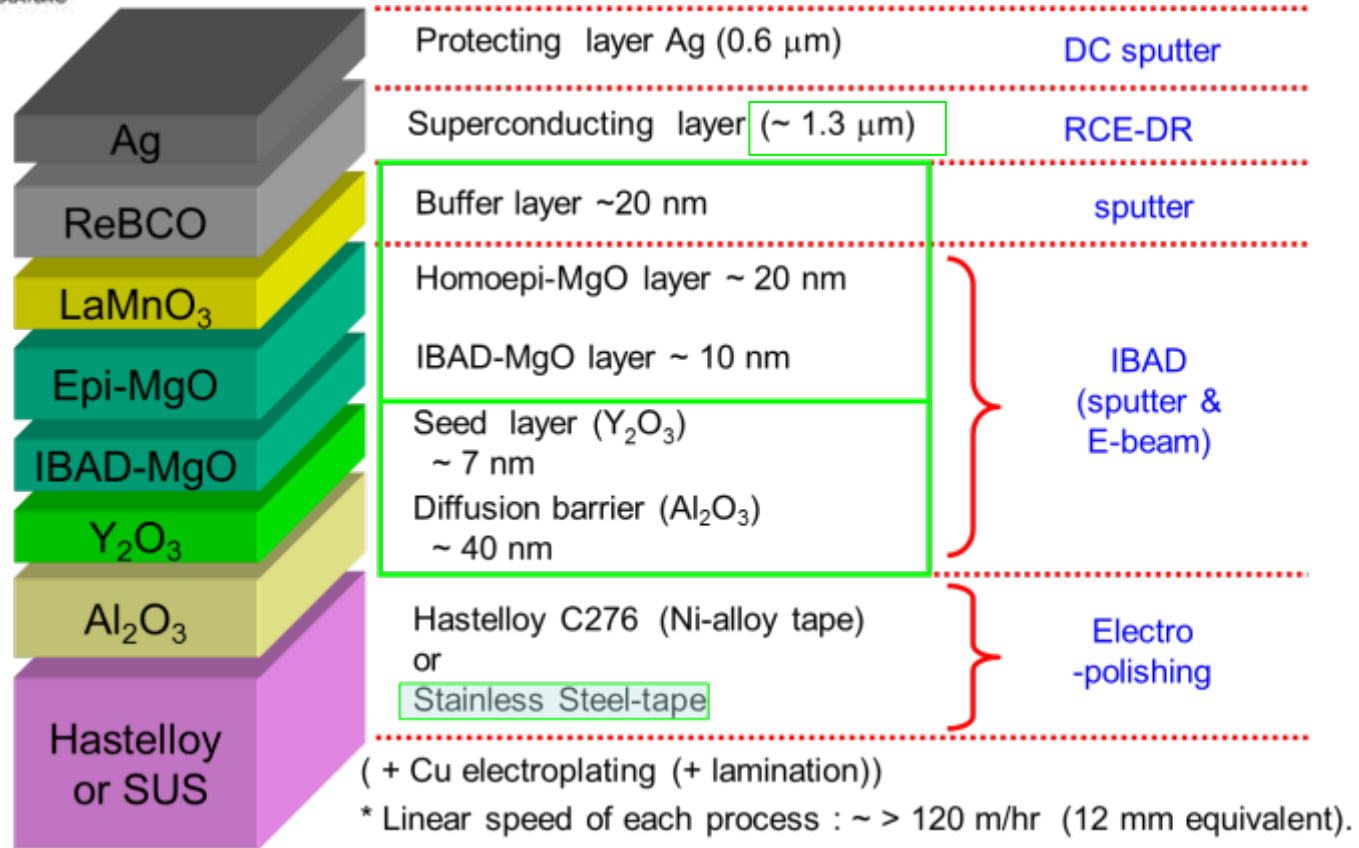
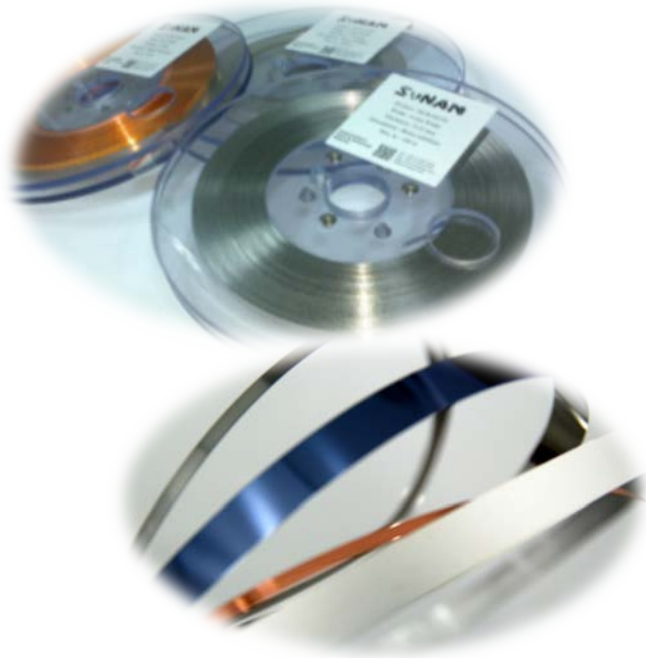
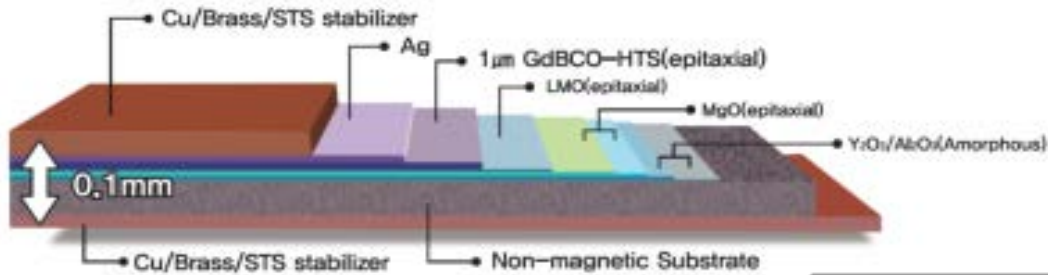
Coated Conductor (2nd G. Wire)

- Superconductor, the main ingredient
- Metal substrate, which gives mechanical strength & flexibility
- Needs good crystallinity for higher current conduction
- Lattice constant mismatch should be small
- Metal diffusion at high processing temperature should be avoided
- Current should be by-passed at quench (breakdown of superconductivity)



Not to scale

Structure

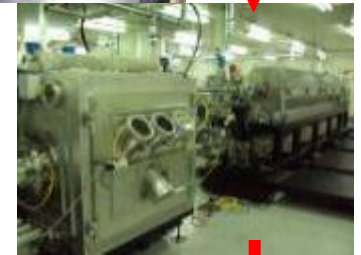


Production Facilities



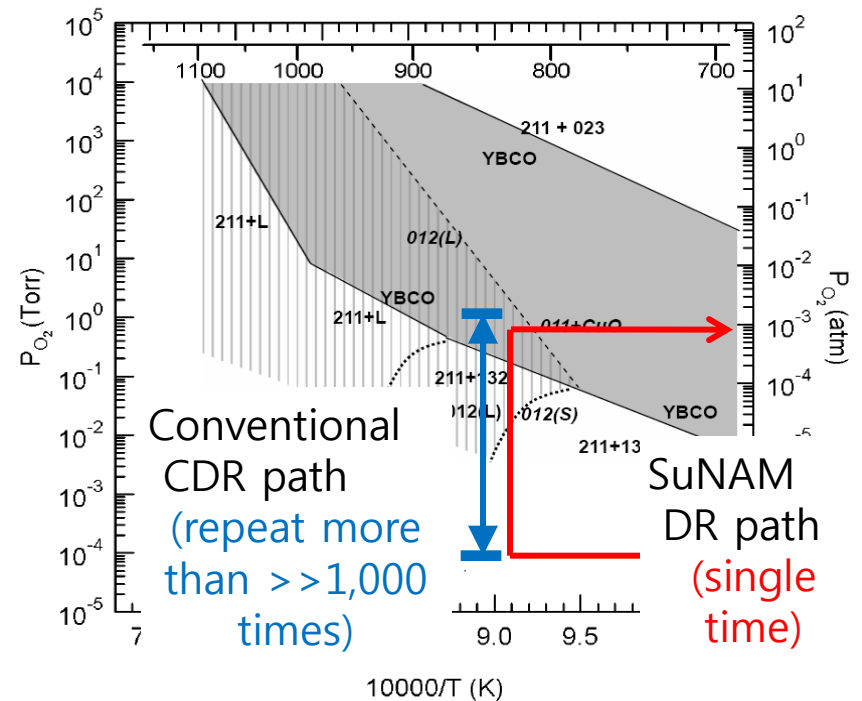
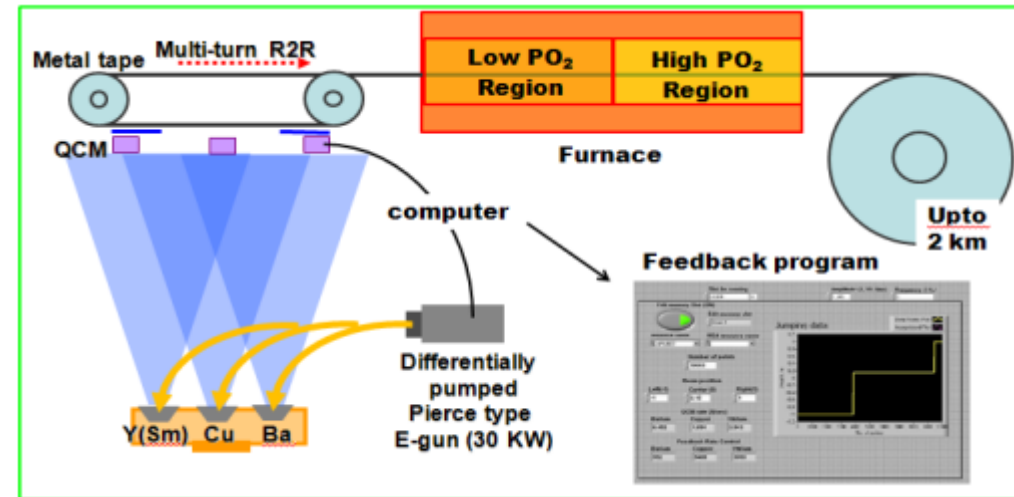
- Site area : 5,500 m²,
Building area : 1,750 m²,
Gross floor area : 3,050 m².

- Class < 10,000 clean
room area : 1,000 m² .

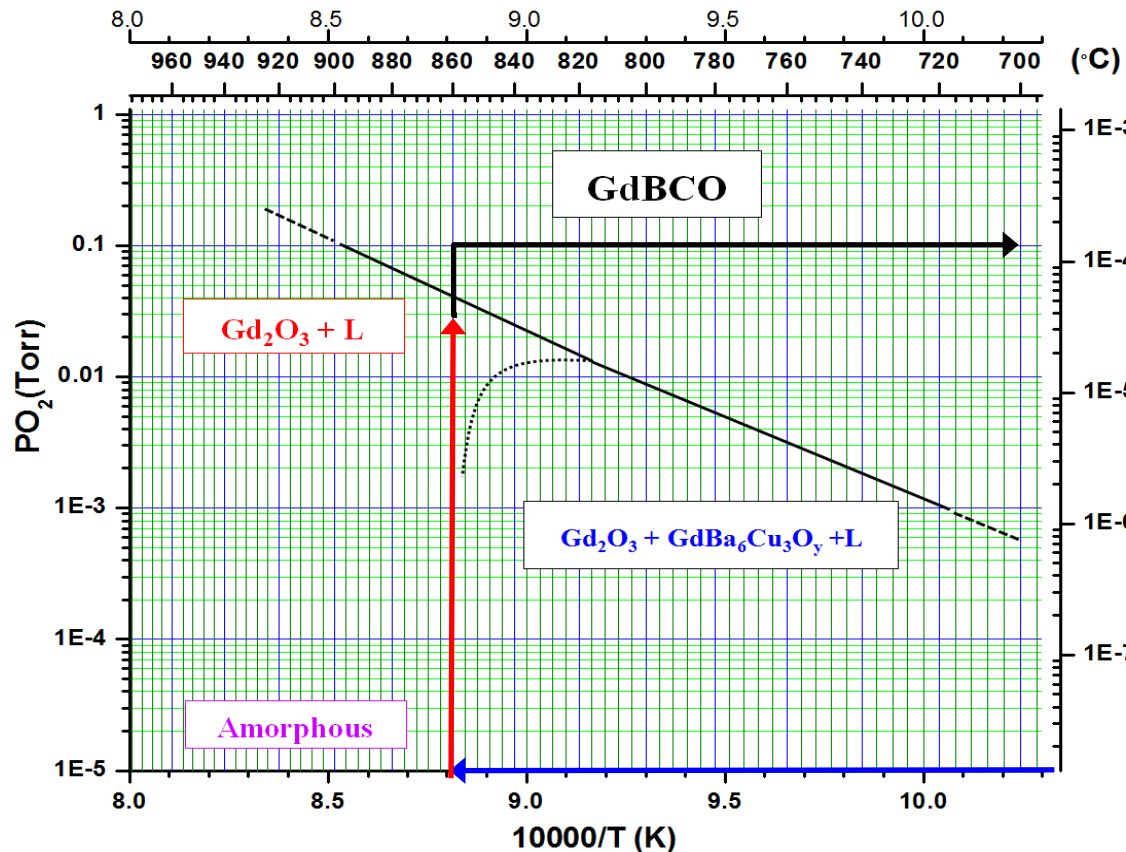


SuNAM RCE-DR process; SC layer

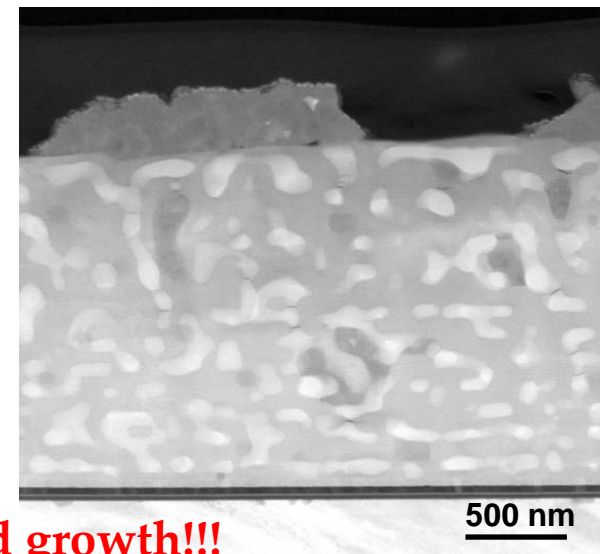
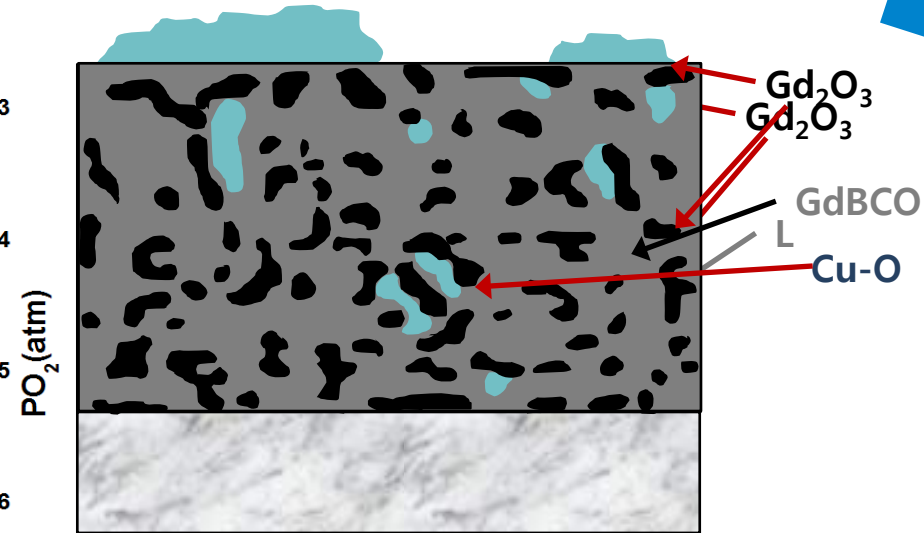
- RCE-DR : Reactive Co-Evaporation by Deposition & Reaction (SuNAM, R2R) : Patented
- High rate co-evaporation at low temperature & pressure to the target thickness ($> 1 \mu\text{m}$) at once in deposition zone (6 ~ 10nm/s)
- **Fast ($\ll 30 \text{ sec.}$) conversion** from **amorphous glassy phase** to **superconducting phase** at high temperature and oxygen pressure in reaction zone
- **Simple, higher deposition rate & area, low system cost**
- **Easy to scale up :single path**



Growth mechanism of the GdBCO film by RCE-DR



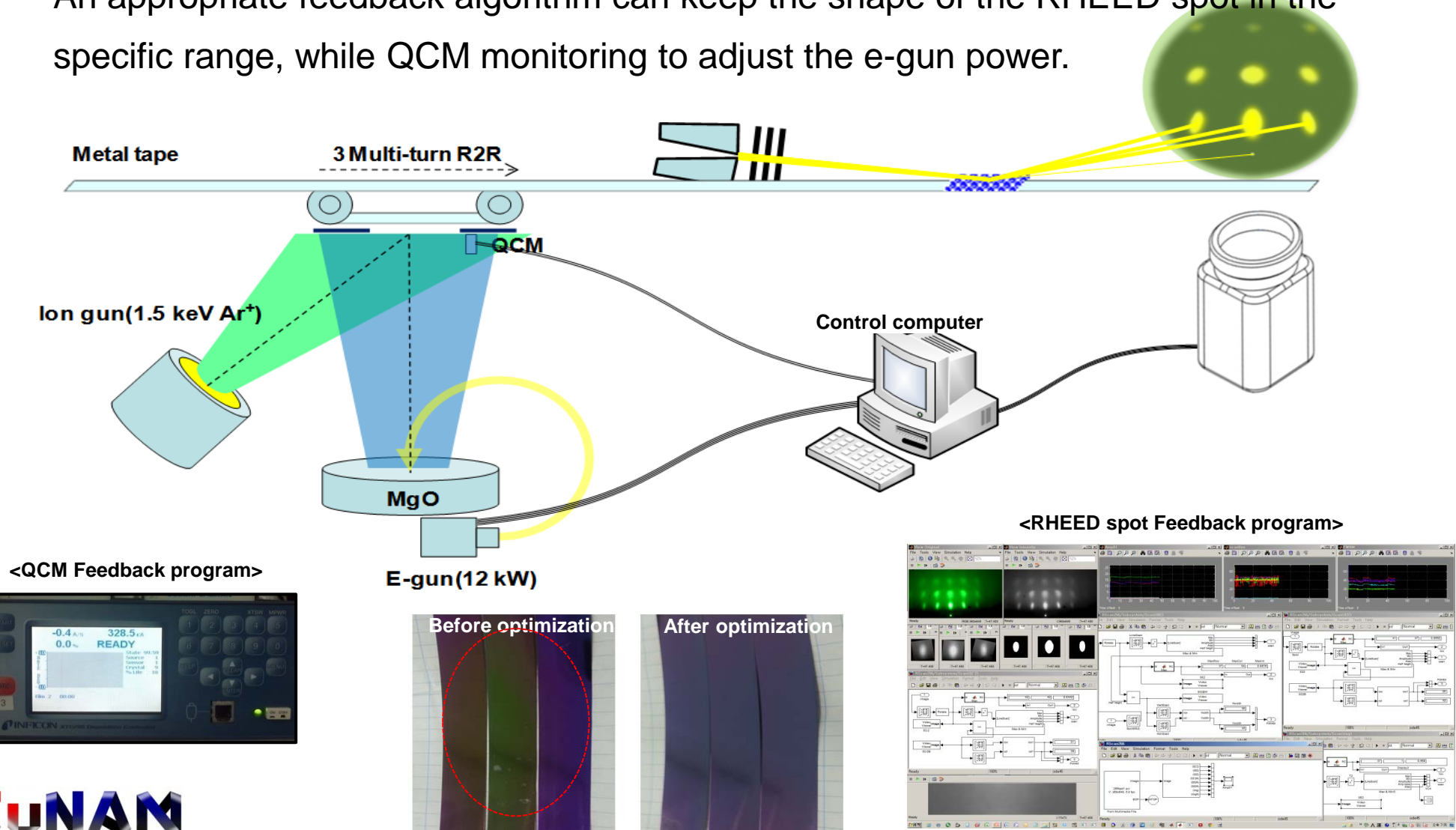
- Very low PO_2 zone ($\sim 10^{-5}$ Torr): **Amorphous Film**
- Lower PO_2 zone (~ 30 mTorr): **Gd₂O₃ + Liquid (< 5 sec)**
- Higher PO_2 zone (~ 100 mTorr): **GdBCO Film (< 20 sec)**



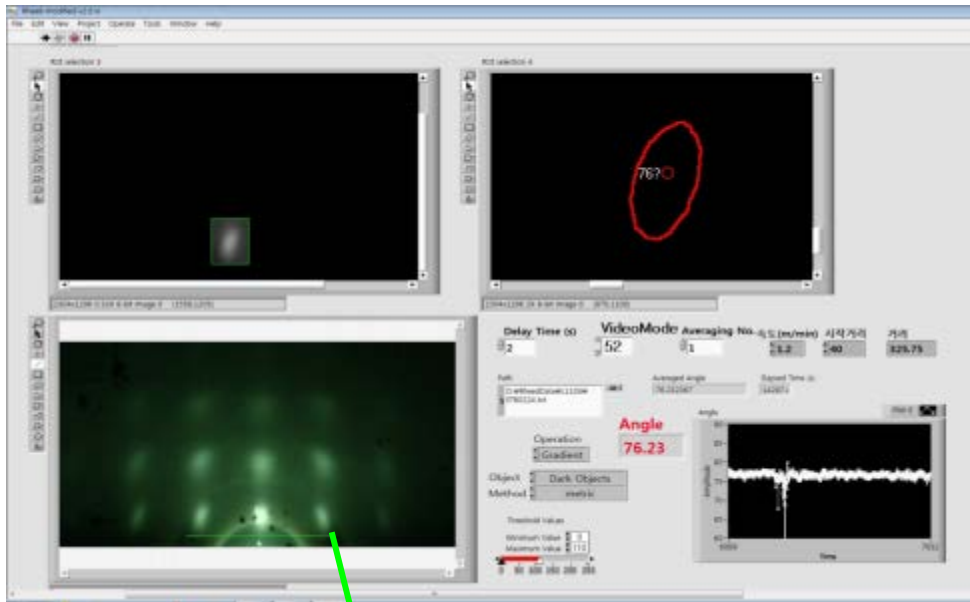
GdBCO growth mechanism: a seeded melt-textured growth!!!

Quality Control : RHEED Vision System on MgO layer for better crystallinity

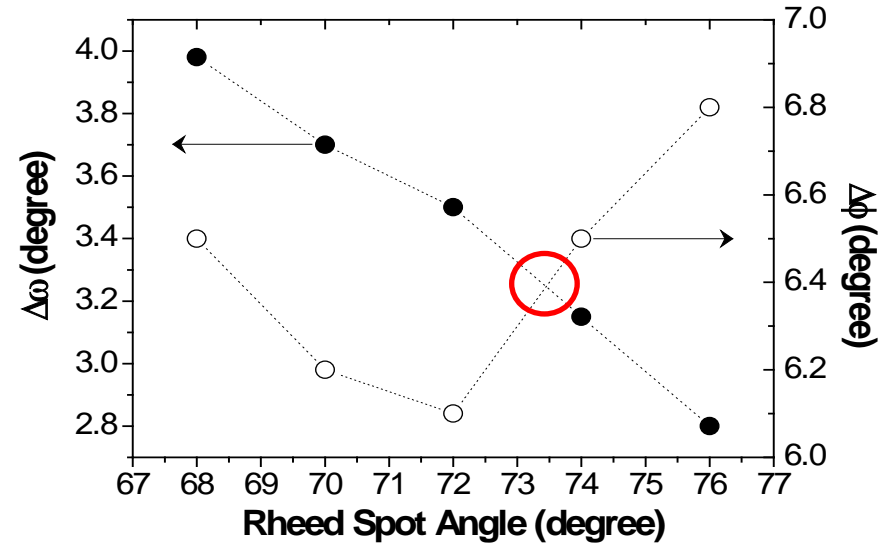
- An appropriate feedback algorithm can keep the shape of the RHEED spot in the specific range, while QCM monitoring to adjust the e-gun power.



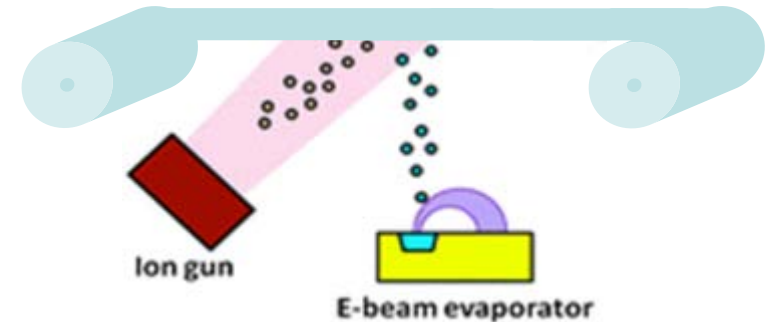
Feedback route based on RHEED spot analysis



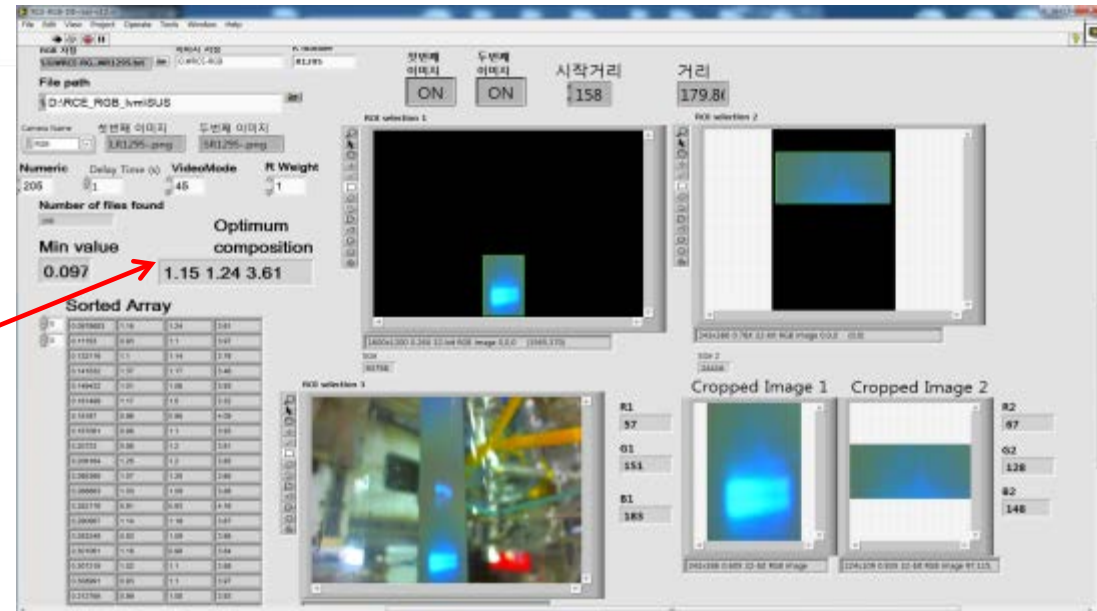
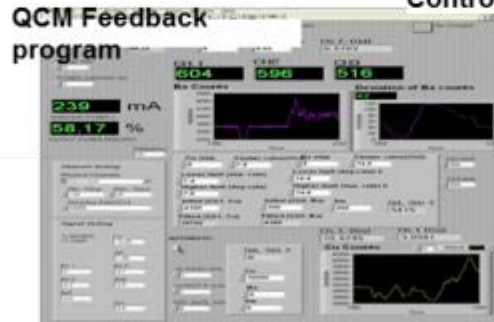
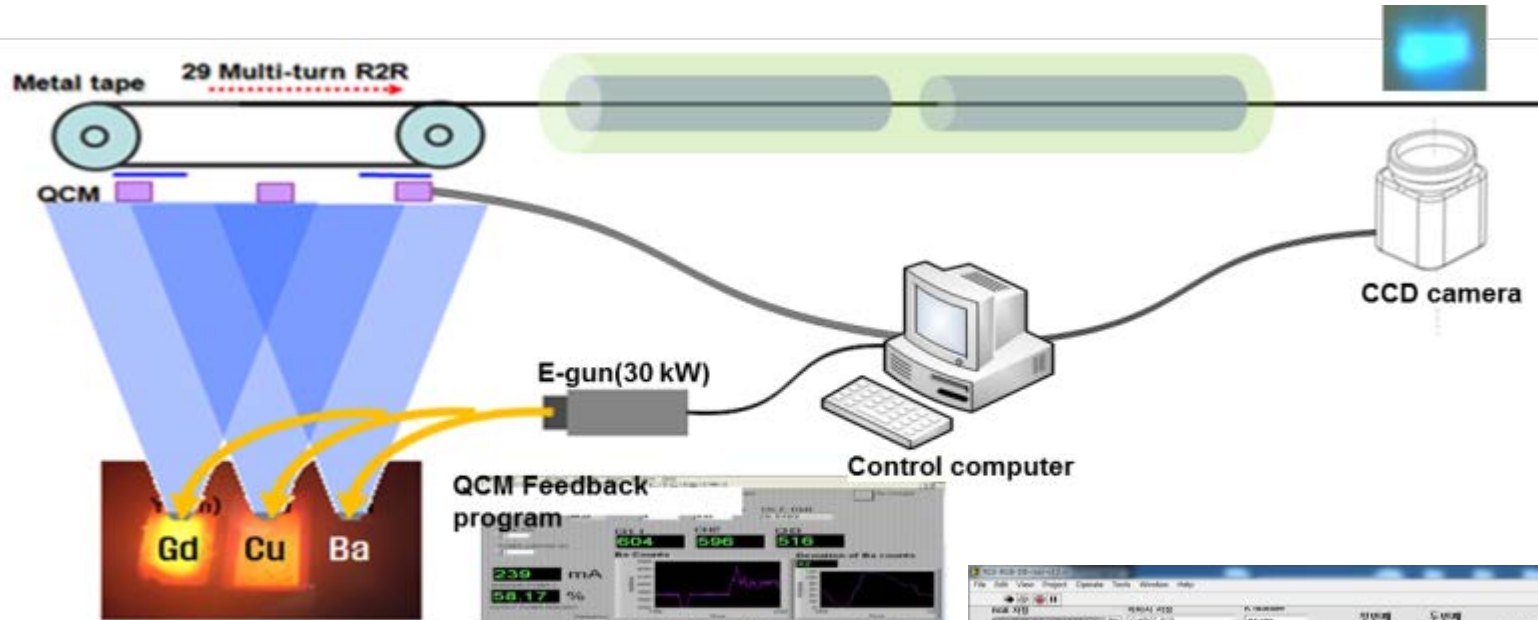
(110) spot



- Because of different evolution of $\Delta\phi$ & $\Delta\omega$, optimization is very important for high quality 2G wire.
- Intensity & tilt angle of MgO (110) spot is one of the most important parameter.



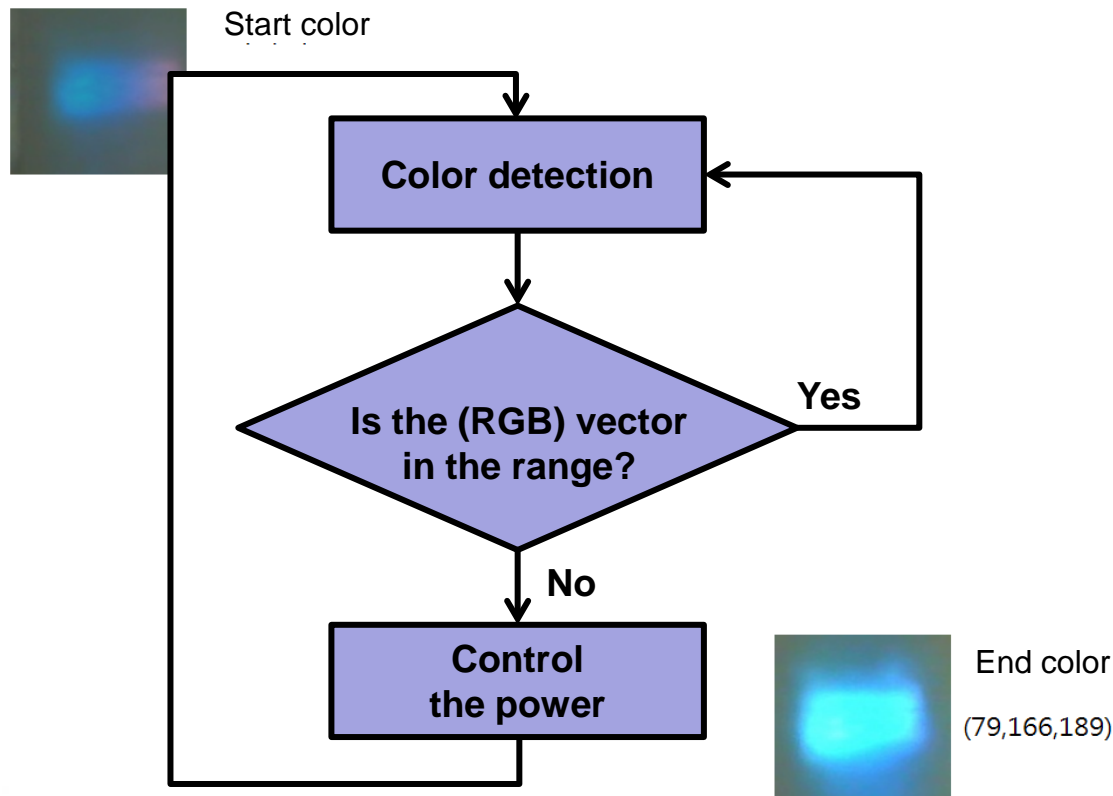
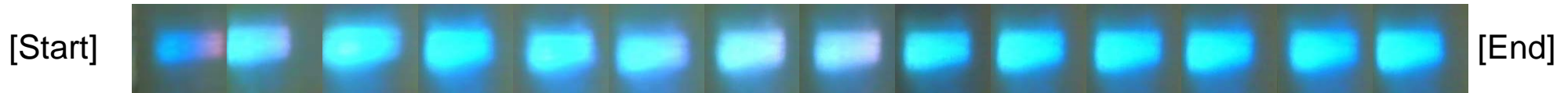
Quality Control : RCE Vision Inspection System on SC layer for precise composition control (higher I_C)



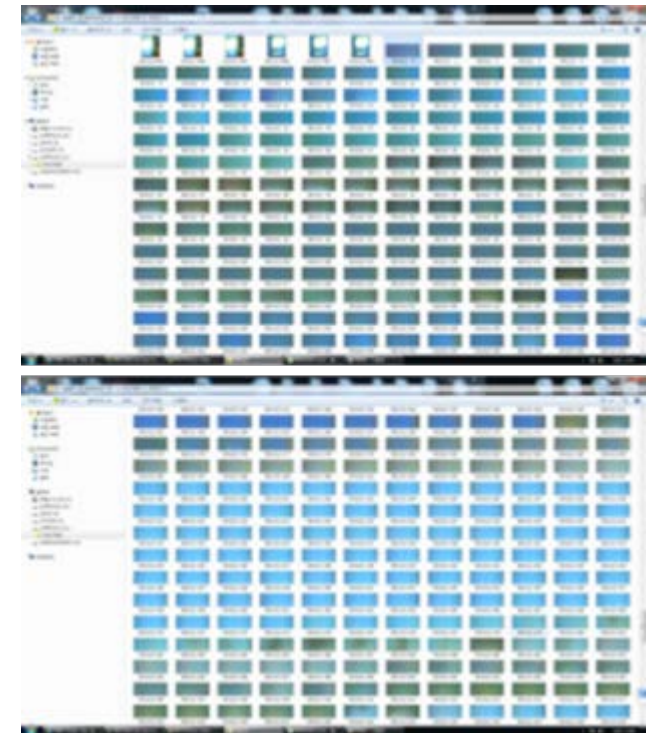
Based on color dependence of composition DB, optimum composition level is automatically controlled by PC. (Slow feedback)

Quality Control : RCE Vision Inspection System

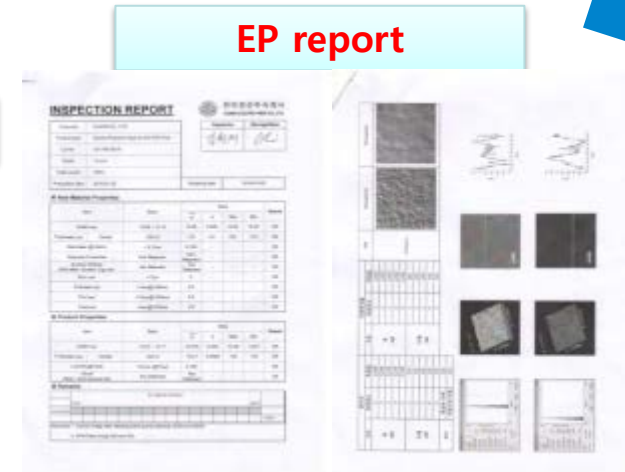
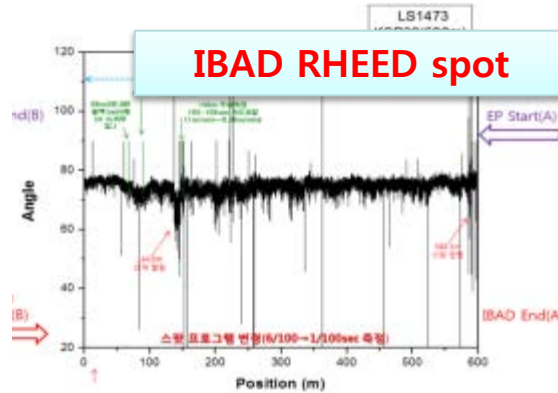
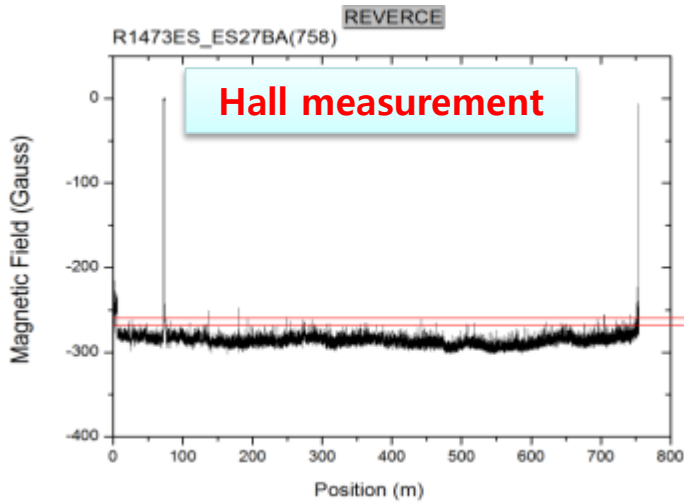
- RCE Vision System will be introduced for increasing the uniformity of composition in RCE-DR process. The control computer takes (RGB) values in three-dimensional vector space which is transformed from the color of the tape surface.



(Composition DB)



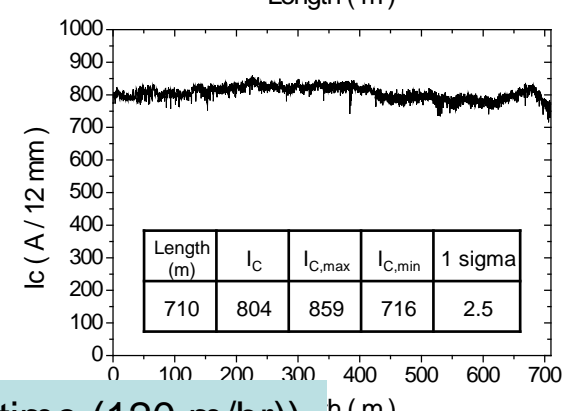
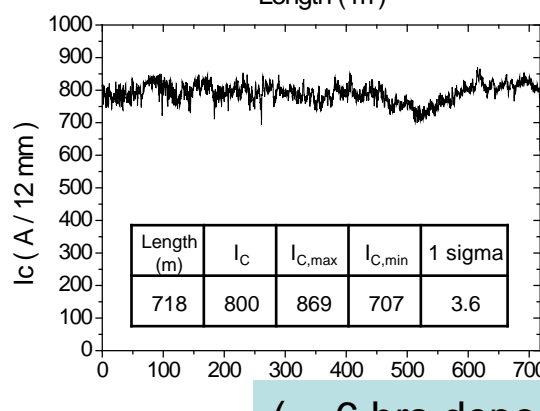
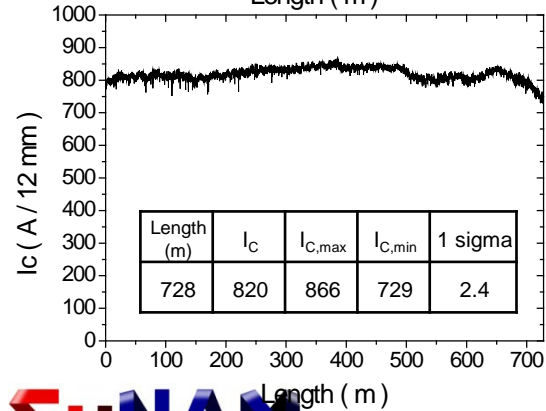
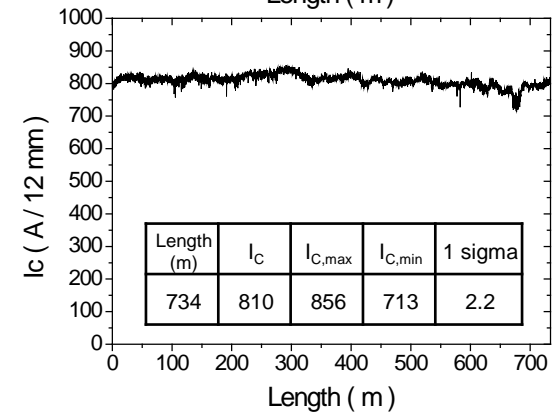
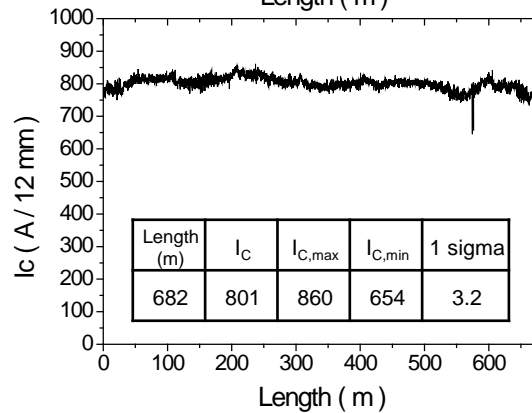
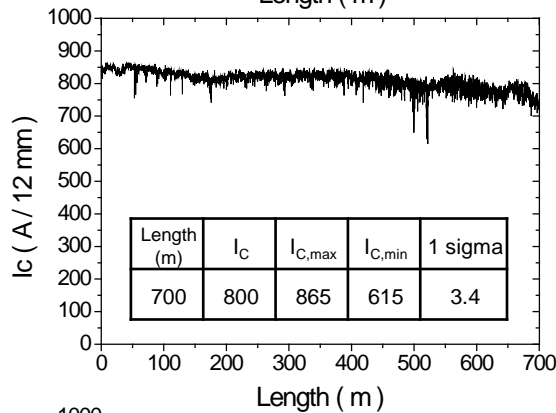
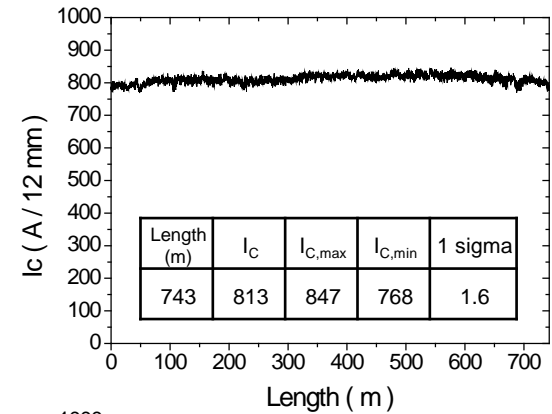
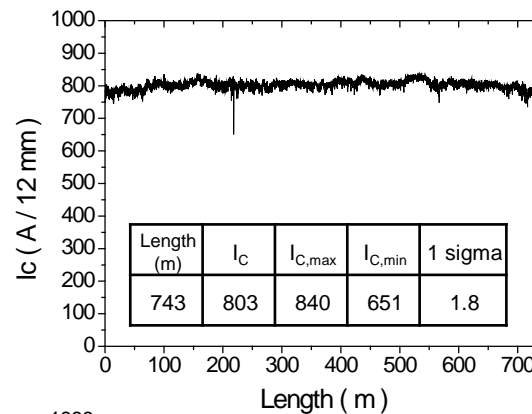
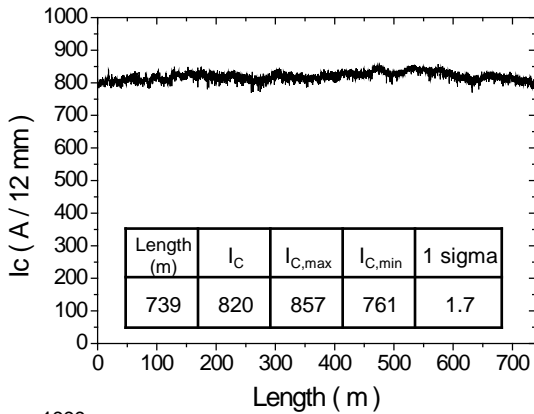
(In-line) QC examples : Root Cause Analysis



PM 01/04/16

NO	TIME	TYPE	WPS-1	WPS-2	Speed	COAT	Deposition rate(A)	Pressure(Torr)	Temperature(°C)	Speed (mm/min)								
1	10:24	EP	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
2	10:28	IBAD	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
3	10:32	RCE	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
4	10:36	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
5	10:40	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
6	10:44	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
7	10:48	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
8	10:52	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
9	10:56	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
10	11:00	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
11	11:04	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
12	11:08	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
13	11:12	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
14	11:16	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
15	11:20	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
16	11:24	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
17	11:28	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
18	11:32	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
19	11:36	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
20	11:40	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
21	11:44	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
22	11:48	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
23	11:52	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
24	11:56	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
25	12:00	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
26	12:04	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
27	12:08	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
28	12:12	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
29	12:16	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
30	12:20	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
31	12:24	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
32	12:28	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
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35	12:40	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
36	12:44	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
37	12:48	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
38	12:52	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
39	12:56	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
40	13:00	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
41	13:04	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
42	13:08	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
43	13:12	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
44	13:16	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
45	13:20	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
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48	13:32	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
49	13:36	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
50	13:40	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
51	13:44	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
52	13:48	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
53	13:52	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
54	13:56	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
55	14:00	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
56	14:04	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
57	14:08	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
58	14:12	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
59	14:16	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
60	14:20	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
61	14:24	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
62	14:28	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
63	14:32	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
64	14:36	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
65	14:40	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
66	14:44	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
67	14:48	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
68	14:52	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
69	14:56	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
70	15:00	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
71	15:04	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
72	15:08	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
73	15:12	Ag sputter	438	1.0	10.0	500	400	4760	4.3	4.3	4.4	130	120	424	100	400	400	1.9
74	15:16	Ag sput																

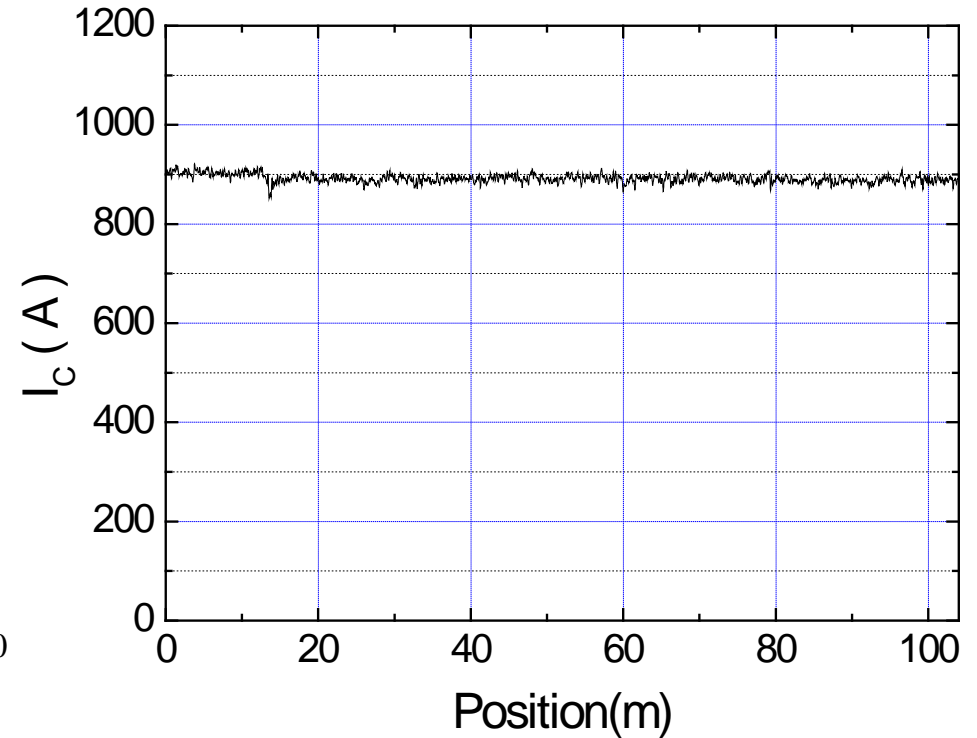
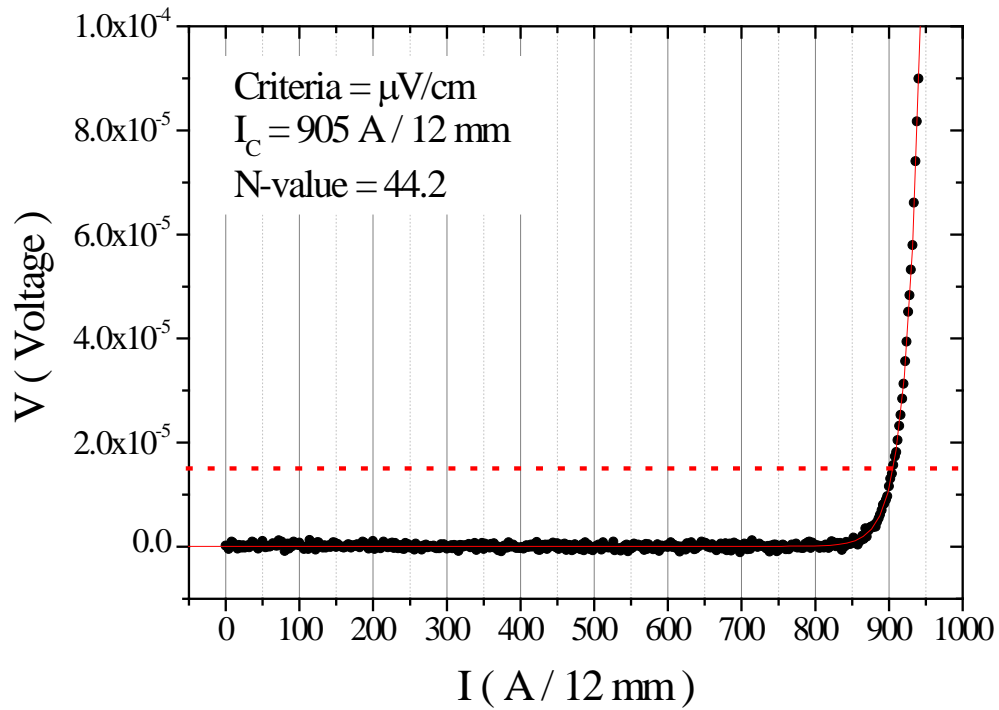
HTS 2G wire performances (daily production)



(~ 6 hrs deposition time (120 m/hr))

Optimized 2G wire performance with 1.6 μm thickness

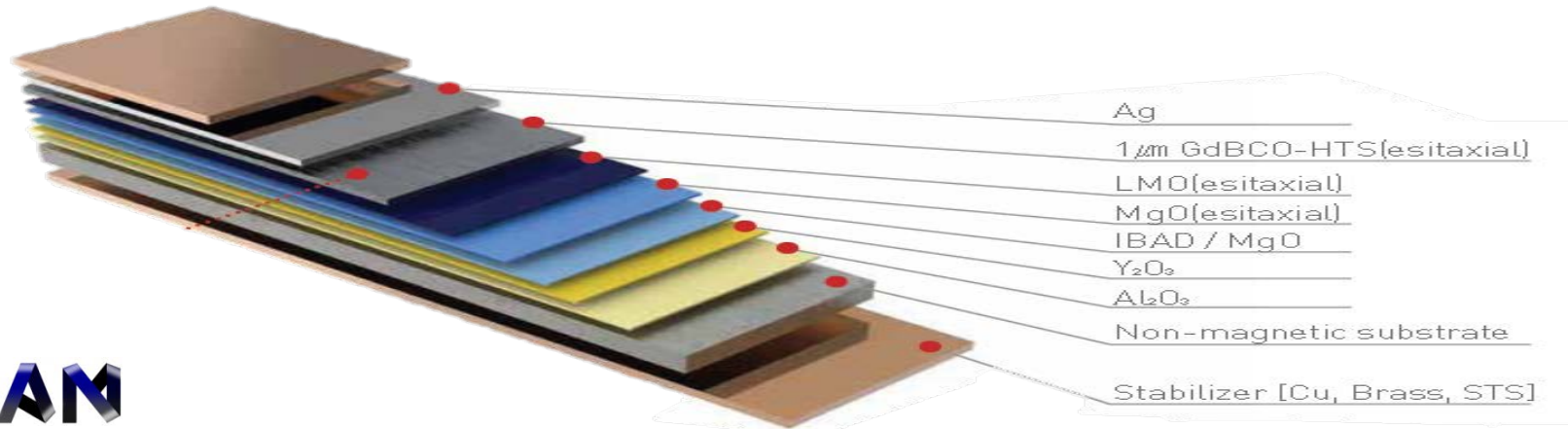
(77 K, s.f.)



SuNAM's 2G HTS Wire

[Specification Table]

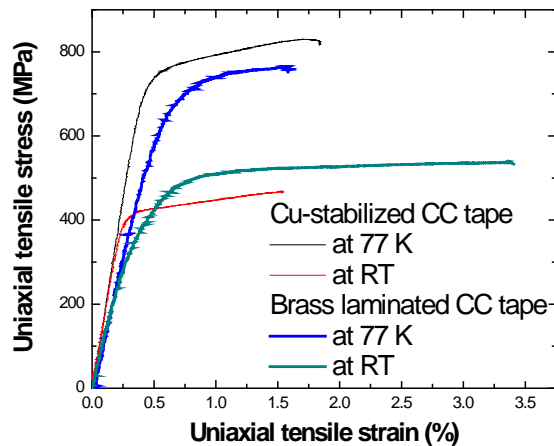
Model	AN	CN	LB/LS/LC	K
Description	Silver(+Cu...) Dry coating	Copper Wet Coating	Brass/STS/Copper Lamination	Polyimide tape(+) Insulation
	Special offer STS metal cladding / Tin coating / Single side lamination			
Substrate	Hastelloy C-276 or Non-magnetic Stainless Steel STS310S			
Width [mm]	Commercial : 4 mm, 12 mm. Special Order : 2 ~ 10 mm multi width is available			
Thickness [mm]	HAS : 0.06~0.07 STS : 0.11~0.12	HAS : 0.09~0.11 STS : 0.14~0.16	Customized	+ 0.1
Final Process	Sputtering	Electro Plating	Lamination	Wrapping
Piece Length	Above 100 m , 200 m , 300 m + without Splice			
Min. Ic @ 77 K S.F.	> 150 / 200 / 250 A + @ 4 mm > 500 / 600 / 700 / 800 A + @ 12 mm			



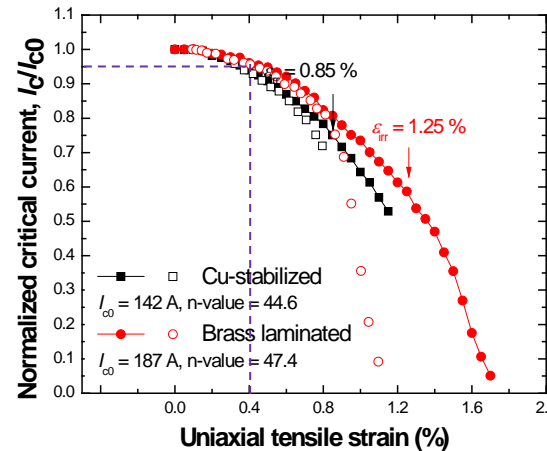
Electro-Mechanical performance of Single Side Brass-Laminated tape

- The CC tapes with brass lamination has the **higher irreversibility of 1.25% strain**.
- **Higher irreversible stress limit of 734 MPa** was shown for the CC tapes with brass lamination, as compared to the Cu stabilized CC tapes.

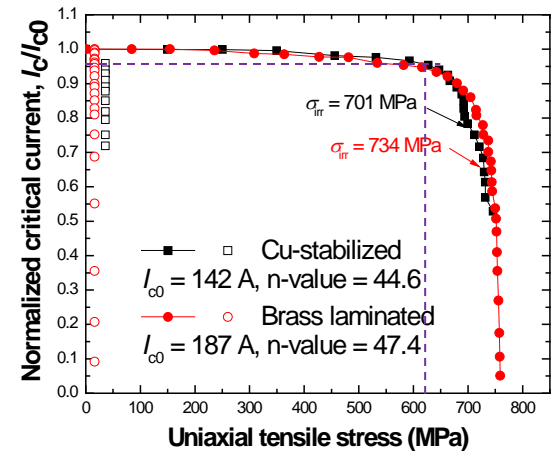
Stress-Strain Curves of Brass-Laminated CC tape



Ic/Ic₀-strain Curves of Brass-Laminated CC tape

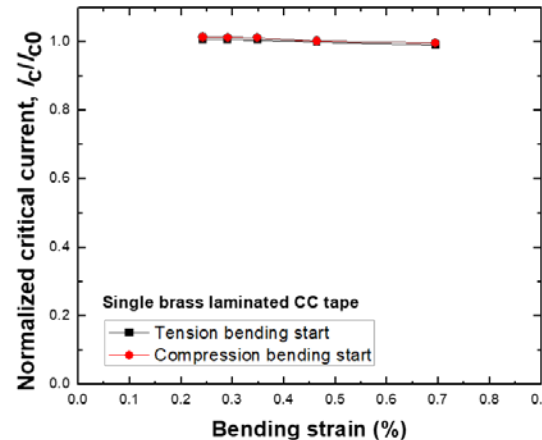
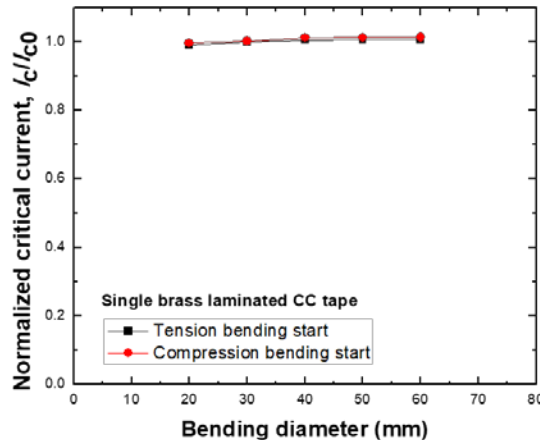
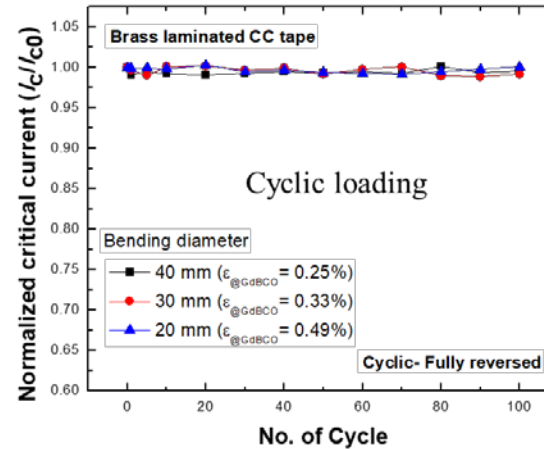
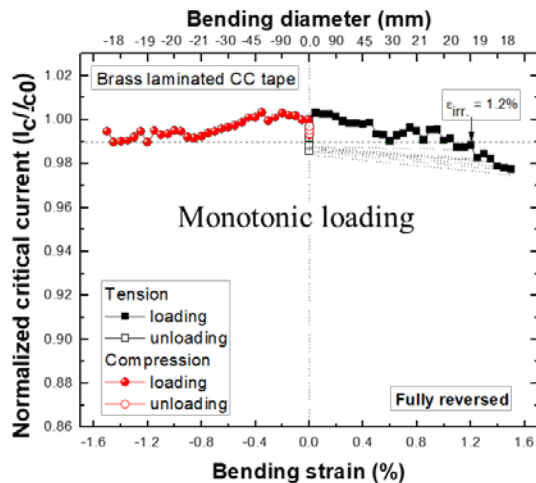


Ic/Ic₀-strain Curves of Brass-Laminated CC tape



CC Tape	At RT		At 77 K				σ _{max} (MPa)
	E (GPa)	σ _y (MPa)	E (GPa)	σ _y (MPa)	ε _{irr.} (%)	σ _{irr.} (MPa)	
Cu-stabilized	160	340	163	589	0.85	701	701
Brass-Laminated	120	450	125	704	1.25	734	668

Electro-Mechanical performance of Single Side Brass-Laminated tape _ Bending



- ϵ_{irr} of 1.2 % was observed in the case of monotonic loading during tension loading.
- No I_c degradation behavior was found on the cyclic tension loading up to **20 mm diameter**.
- Laminated CC tapes showed no I_c degradation up to **20 mm ($\epsilon_{@GdBCO} = 0.25\%$)** bending diameter.

Published paper

Evaluation of the electromechanical properties in GdBCO coated conductor tapes under low cyclic loading and bending

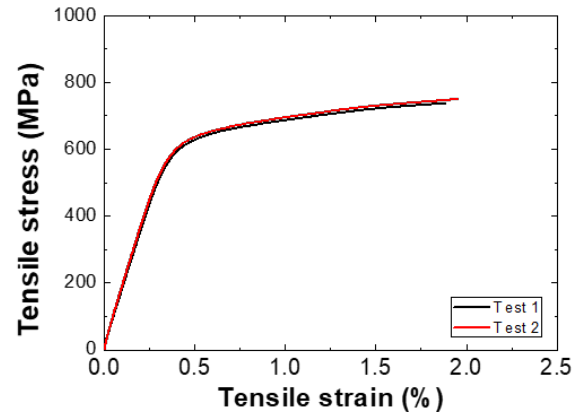
Hyung-Seop Shin, Alking Gorospe, Zhierwinjay Bautista and Marlon James Dedicarria

Supercond. Sci. Technol. 29 (2016) 014001 (12pp)

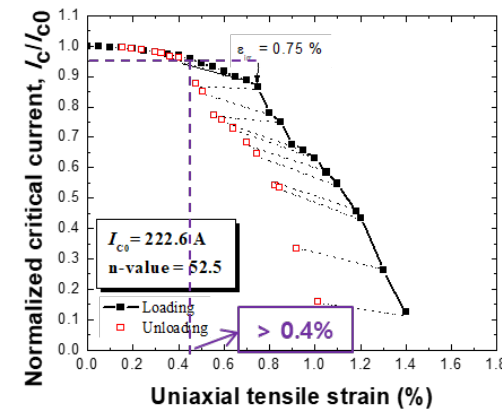
Electro-Mechanical performance of Sn/Cu stabilized tape

- Sn/Cu stabilized GdBCO CC tape exhibited
 - an irreversible strain limit, $\epsilon_{irr} = 0.75\%$
 - an irreversible stress limit, $\sigma_{irr} = 641$ MPa, respectively.

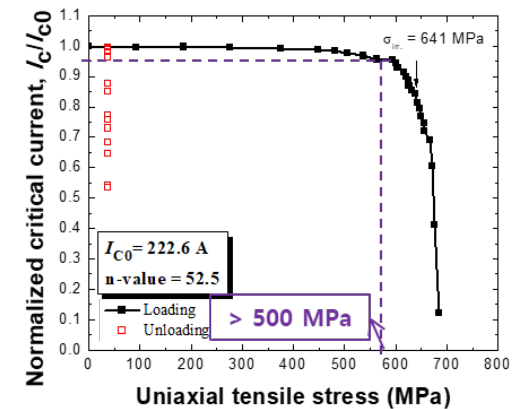
Stress-Strain Curves of Sn/Cu Stabilized CC tape



I_c/I_{c0} -strain Curves of Sn/Cu Stabilized CC tape



I_c/I_{c0} -strain Curves of Sn/Cu Stabilized CC tape



Sample		Dimension, Width/Thickness [mm]	Yield strength (MPa)	Ultimate Tensile strength (MPa)
Sn/Cu stabilized CC tape	Test 1	4.05/0.138	644	829
	Test 2	4.05/0.137	650	936

Continuous bending & other mechanical tests

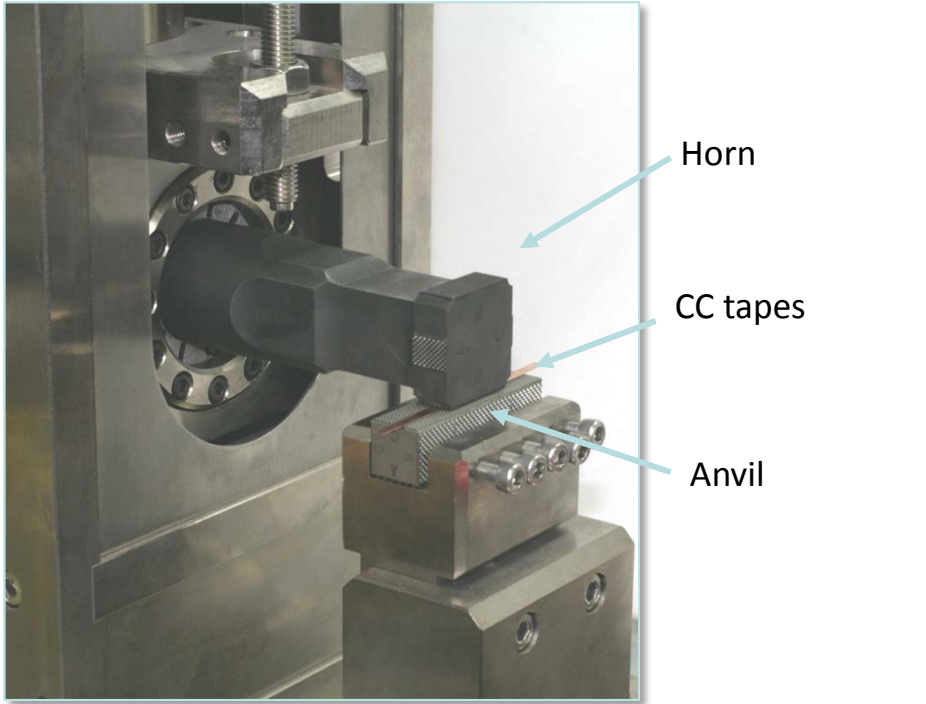


[Continuous Ic measurement system with Bending-Double bending rollers]

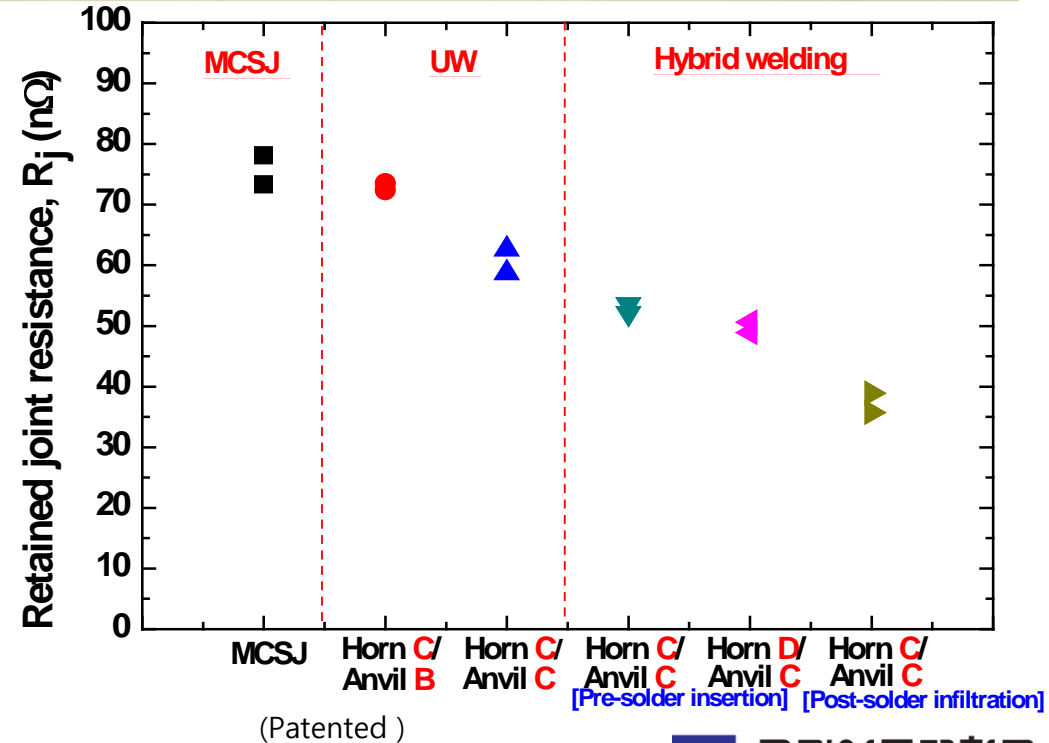
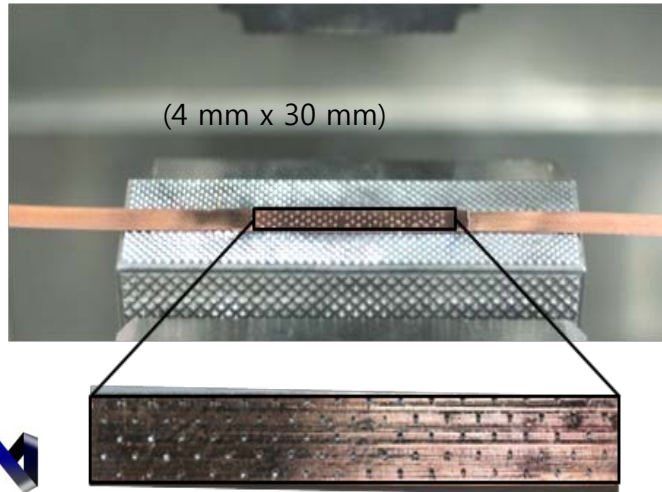
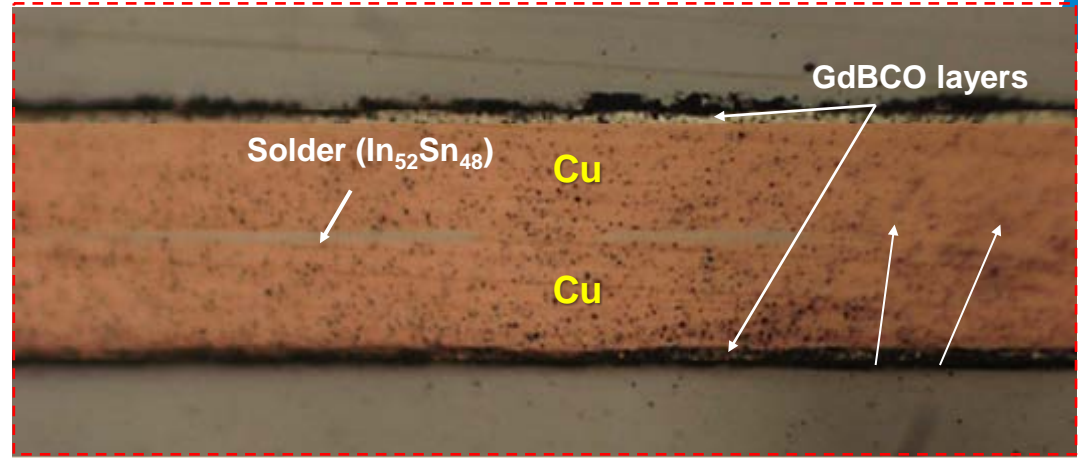


[Sample based Stranding-Thermal cycle test]

Simple, Fast & Reliable Hybrid Ultrasonic Welding joint method



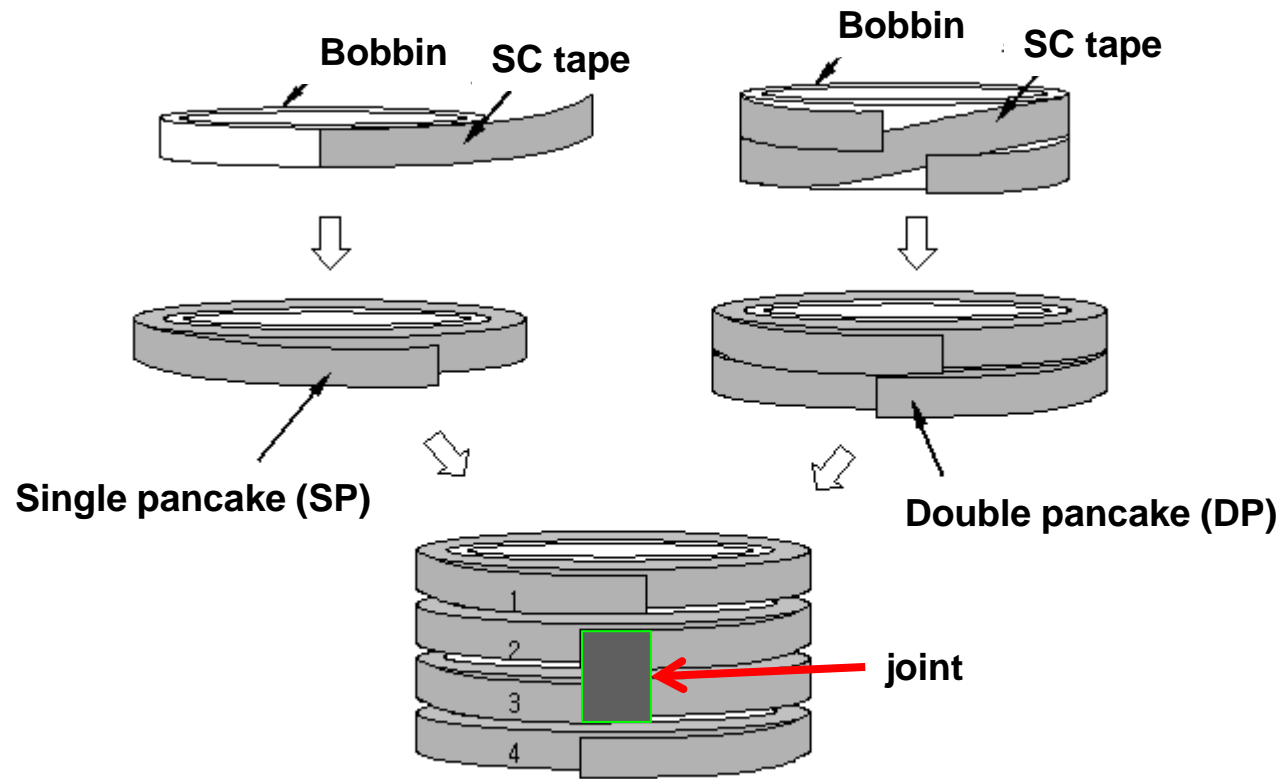
Ultrasonic welder machine



Magnet & Coil

(Double) Pancake Coil

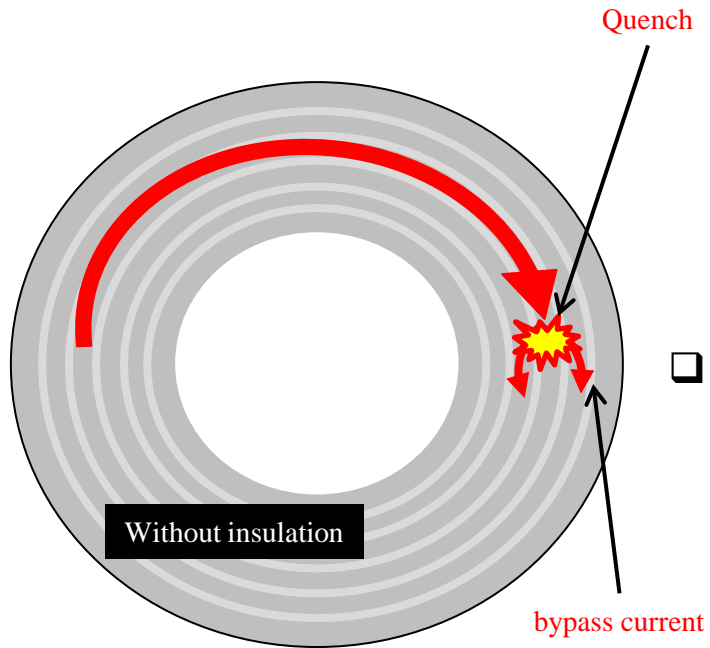
- Pancake winding is adopted due to tape-form of HTS wire



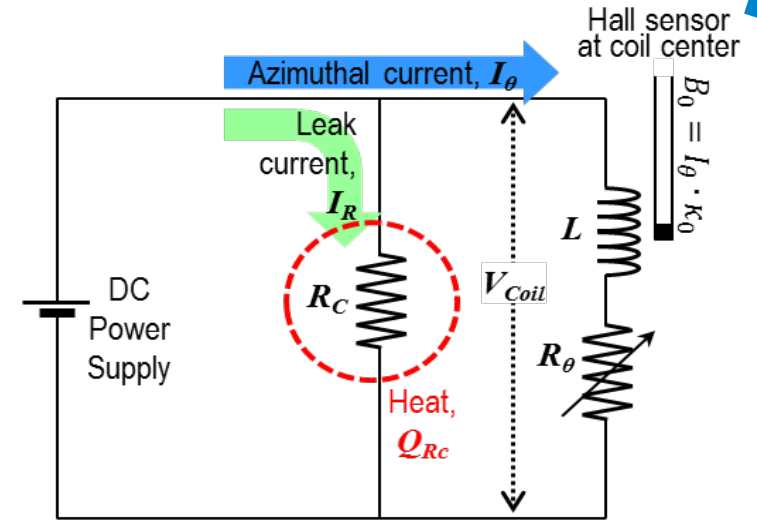
Coil with 4 Single Pancakes or 2 Double Pancakes;
For SP case, SP 1-2 & 3-4 are joined inside, 2-3 outside.

- Layer winding is also exercised for better uniformity

NI-winding technic – No insulation



□ **"Automatic bypass"**
of the exceeding
current and better
protection to quench



$$Q_{RC} [W] = I_R^2 \cdot R_C$$

where, $I_R = I_{PS} - I_\theta = I_{PS} - \frac{B_0}{k_0}$

No-insulation winding technic :

Pros :

- ✓ Compactness : without thick stabilizer
- ✓ Strong mechanical strength : without soft insulation material
- ✓ Self protection : automatic bypass
- ✓ Rapid quench propagation

Cons :

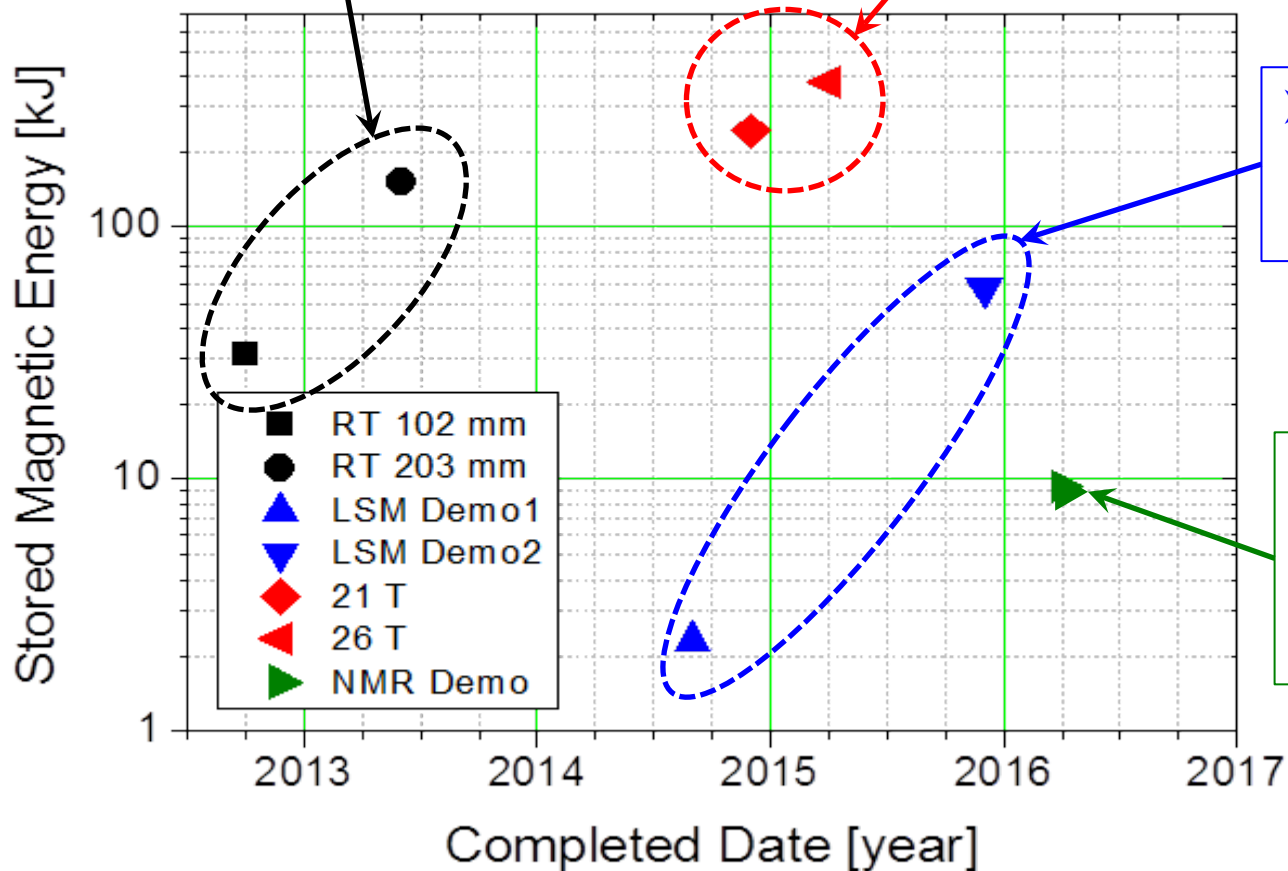


Charging time delay.
**(excess heat generation/
Impractically slow for
charging)**

Progress in NI Magnet at SuNAM

- Wide RT bore magnet
 - Over 4 [T] at center
 - For I_C measurement
 - Cryogen-free

- High field magnet
 - Over 20 [T] at center
 - Liquid helium cooling



- Racetrack magnet
 - For motor application
 - Cryogen-free

- Homogeneity magnet
 - For NMR application
 - Over 3 [T] at center
 - Cryogen-free

Long-Term Operation (203mm Magnet)

- Cooling time (operation)
: 3 years
- Total field charging time
: > 200 times, **> 700 hours**
- I_C -B-T- θ measuring times
: > 4,000 points
- Quenches
: more than 6 times

I_C measurement
insert cryostat

203mm RT
4T magnet



< I_C (B-T- θ) measurement system >

HTS magnet for 10kW generator

Performance Analysis of a 10-kW Superconducting Synchronous Generator

A-Rong Kim, Kwang-Min Kim, Heecheol Park, Gyeong-Hun Kim, Tae-Joon Park, Minwon Park, Seokho Kim, Sangjin Lee, Hongsoo Ha, Sangwon Yoon, and Hunju Lee

Abstract—POSCO and the Research Institute of Industrial Science and Technology developed a 10-kW superconducting synchronous generator using high-temperature superconducting wire. The generator consists of four-pole racetrack-type superconducting coils using GdBCO wire for rotor and 24 slots copper windings for stator. The rated power of the generator was 10 kW at 600 r/min, and the operating temperature was 30 K by thermosyphon cooling method using liquid neon. The output power was measured when the generator was connected to a vector motor, and the detailed results were discussed in this paper.

Index Terms—GdBCO, liquid neon, rotating machine, superconducting generator.

I. INTRODUCTION

BECAUSE of increasing the electricity demands, larger power systems are expected with high efficiency. To in-

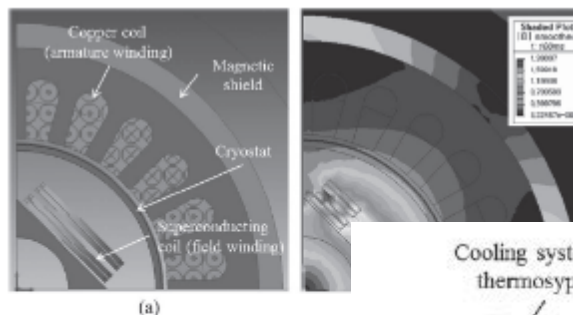
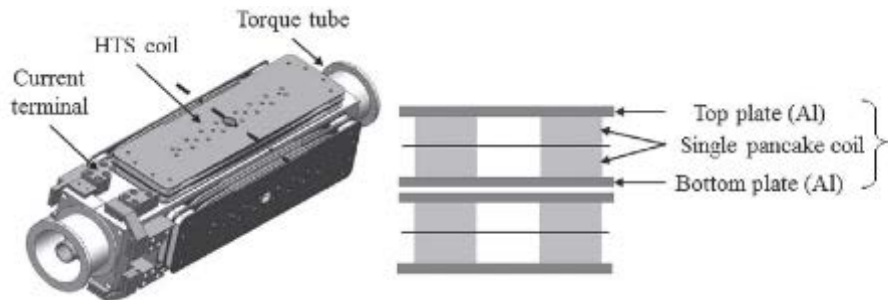
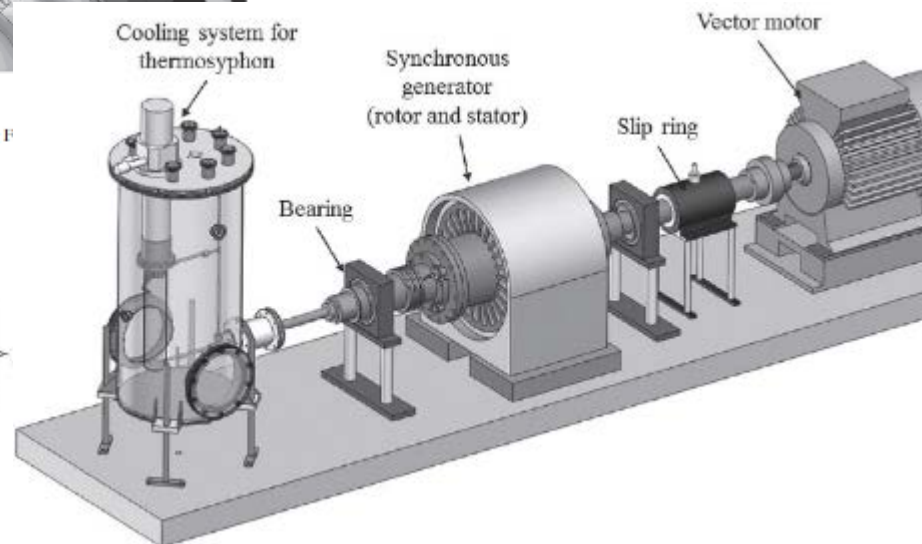


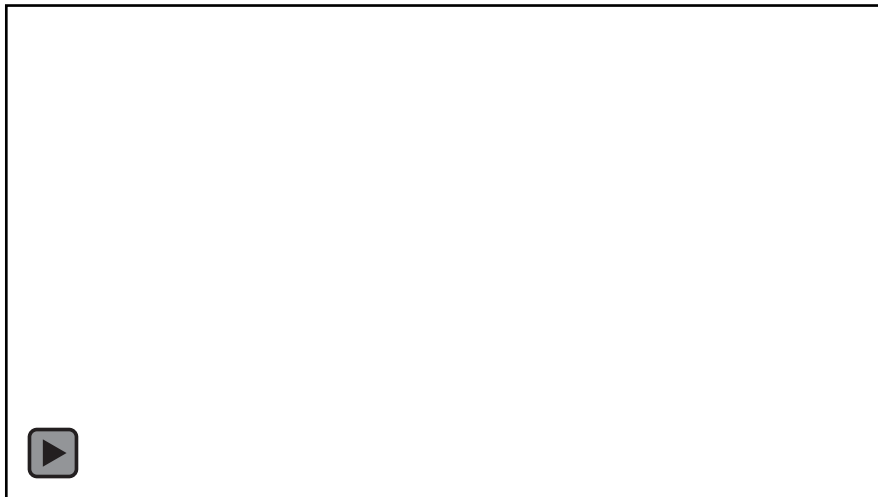
Fig. 1. Design results of the generator using F area. (b) Magnetic field distribution.



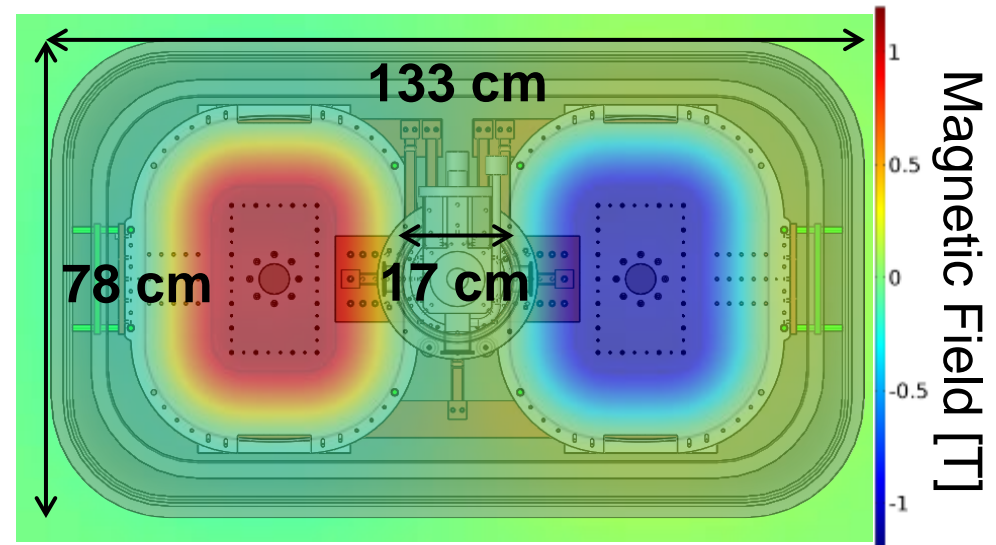
Racetrack Coil for Motor Application

Ref.) C.-B Park *et al*, "Development of a Small-Scale Superconducting LSM...", *IEEE Trans. Energy Conversion*

- 2 Poles and 3 double pancake coils per pole
- Peak field on the rail : > 1 Tesla (65 mm apart from magnet bottom)



< Linear synchronous motor >
(small coil)



Field profile at AC copper coil on track

- ✓ Smooth but powerful movement
- ✓ No voltage fluctuation or field decay

HTS magnet for LSM

This article has been accepted for publication in a future issue of this journal, but has not been fully edited. Content may change prior to final publication. Citation information: DOI 10.1109/TEC.2016.2577058, IEEE Transactions on Energy Conversion

Development of a Small-scale Superconducting LSM using Gd-Ba-Cu-O High-Temperature Superconducting Wire

Chan-Bae Park, *Member, IEEE*, Chang-Young Lee, *Member, IEEE*, Sangwon Yoon and Seokho Kim

Abstract—In this research, a 600 km/h-class high-speed train with wheel-rail support and a linear synchronous motor (LSM) propulsion system is being considered. Prior to the development of superconducting LSM for propulsion of 600 km/h-class high-speed trains, pre-performance validation through a small-scale prototype is required. Therefore, a small-scale 7 kW-class superconducting air-core-type LSM prototype was designed, one that includes a superconducting magnet with 2 poles. High-temperature superconducting (HTS) wire of the Gd-Ba-Cu-O series was used for the magnet. Next, the various characteristics of the designed model were estimated through a numerical approach, with the finite element method (FEM). Finally, a small-scale superconducting LSM prototype was produced and installed in a bogie on a 10-m track. A performance test of the superconducting magnet and a no-load induced voltage and thrust measurement test of the small-scale superconducting LSM were completed. The effectiveness of the proposed superconducting LSM design techniques and design model was verified.

Index Terms— Linear synchronous motor, LSM, High-temperature superconducting, HTS, High-speed train

propulsion system that is based on rotary-type traction motors, it is quite difficult to operate trains with an ultra-high speed of 500 km/h or beyond. In order to overcome the speed limitations of the trains due to the adhesive drive propulsion system, a magnetic levitation vehicle (Maglev) that uses a linear motor propulsion system has been invented [3]. At present, the fastest train in the world is Japan's superconducting Maglev, at a high speed of 581 km/h. Japan is almost finished experimenting on the test track and it will be ready for commercial operation [1]. However, the Maglev's commercial operations are being delayed due to numerous issues, including technical and economic problems. The hybrid-type train system is emerging as an alternative to the conventional high-speed train and the Maglev system [4]. The hybrid-type train system incorporates the strengths of the wheel-rail supported adhesive drive propulsion system and the Maglev system. Although the hybrid-type train system is based on a wheel-rail guided system, a linear motor is used for propulsion instead of a rotary motor. The non-adhesive drive propulsion system by a linear motor is able to overcome the speed limitation of the conventional high-speed train [5]. Figure 1 shows a conceptual diagram of an

TABLE I
DESIGN RESULTS OF THE SMALL-SCALE SUPERCONDUCTING LSM MODEL

Contents	Value
Output power	7 kW
Max. thrust	118 N
Max. operating frequency	2.8 Hz
Length of test track	10.08 m
Pole-pairs in test track	12
Turns/Pole (Armature coil)	20 Turns
Max. current/Phase for whole track	44 A _{eff}
Resistance/Phase for whole track	0.431 Ω
Air-gap / Pole pitch	65 mm / 420 mm
Pole numbers (SC magnet)	2
Required MMF (SC magnet)	72 kA-Turns
Operating current (SC magnet)	120 A

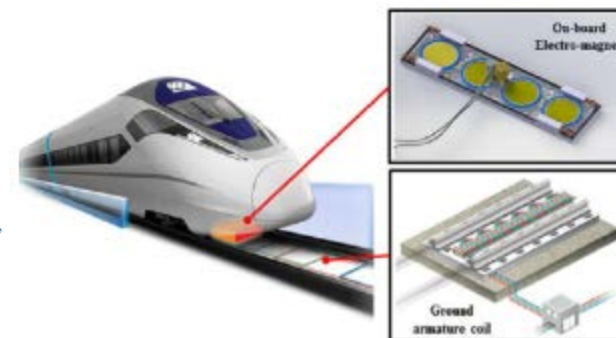
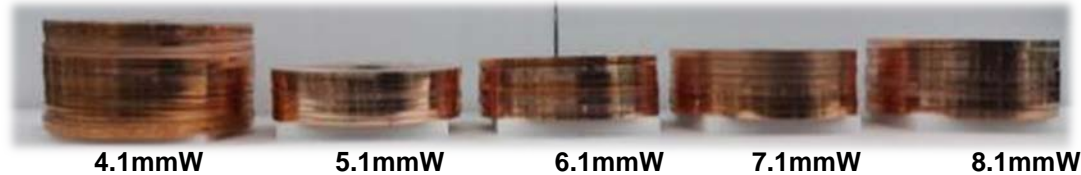


Fig. 1. Conceptual diagram of the ultra-high speed 600 km/h trains [4]

26.4 T all 2G wire one-body(non-nested) magnet

No-insulation, multi-width, and compact !

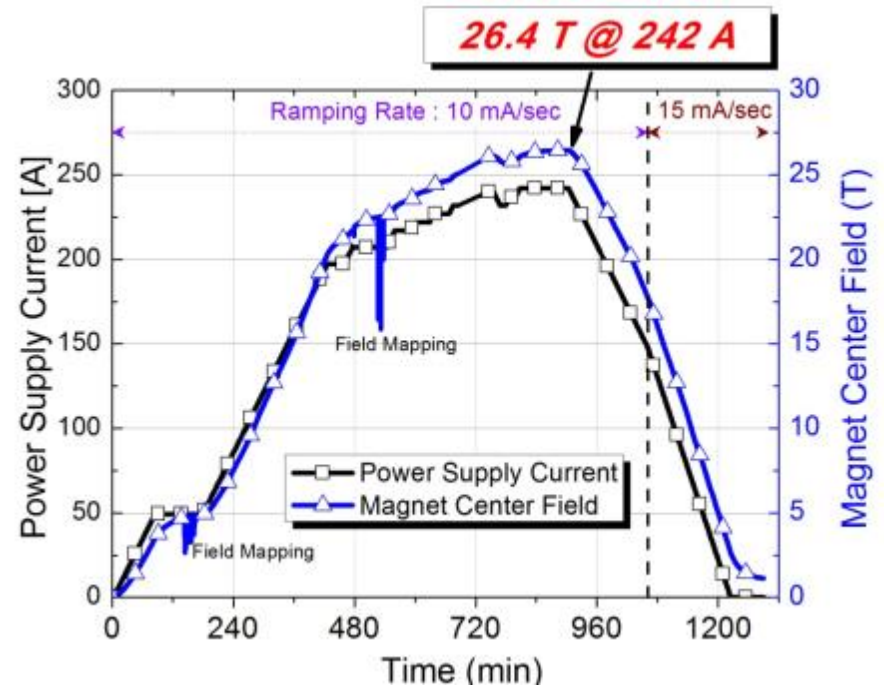
- ✓ Multi-width Double Pancake Coils



- ✓ Stacked Double Pancake Coils



- ✓ Fully assembled



Immersed in liquid Helium

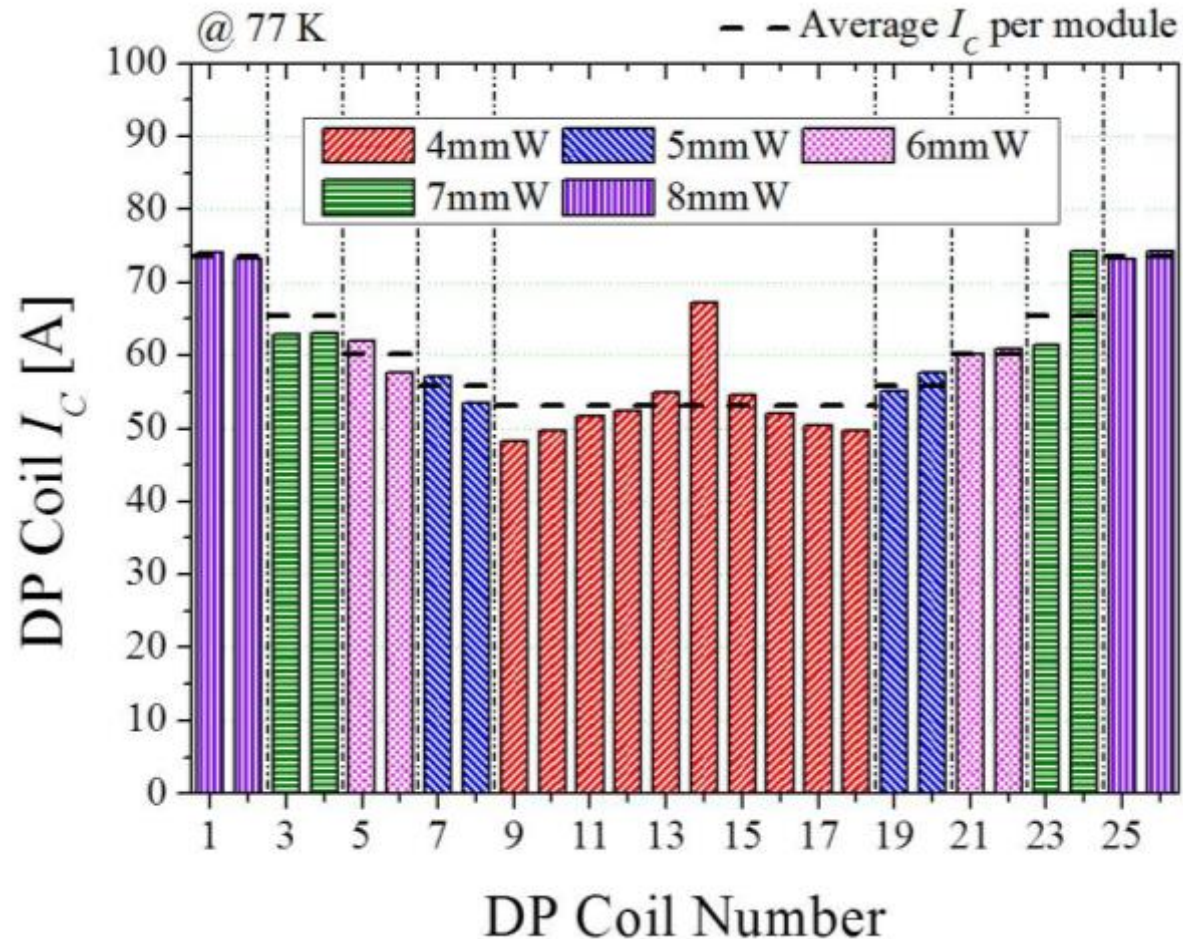
Key Parameters of 26 T Magnet

Ref.) S. Yoon *et al*, "26T 35mm all-GdBa₂Cu₃O_{7-x} multi-width no-insulation..." *Supercond. Sci. Technol.*

Parameter		M1	M2	M3	M4	M5
Tape Width	[mm]	4.1	5.1	6.1	7.1	8.1
I.D.; O.D.	[mm]	35.0; 171.8				
Height	[mm]	327				
No. of DP		10×1	2×2	2×2	2×2	2×2
Turn per DP (Avg.)		946				
Operating Current, I_{OP}	[A]	242				
Operating Temp., T_{OP}	[K]	4.2 (in liquid helium)				
Magnetic Field	[T]	26.4				
Inductance	[H]	12.3				
J_e @ I_{OP}	[A/mm ²]	404	327	293	247	221
$B_{perp.}$ @ I_{OP}	[T]	1.54	1.59	1.82	2.08	3.68

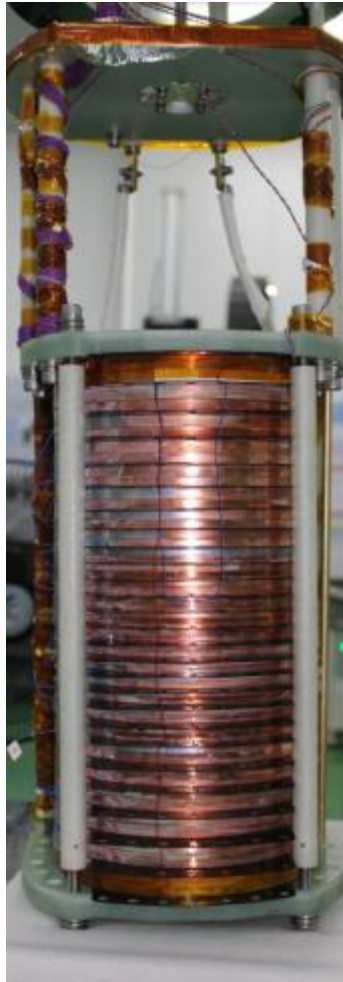
Coils are arranged by 77 K I_c

- ✓ Critical current (I_c) of each DP coil with a 0.1- μ V/cm criterion was measured in a bath of liquid nitrogen at 77 K



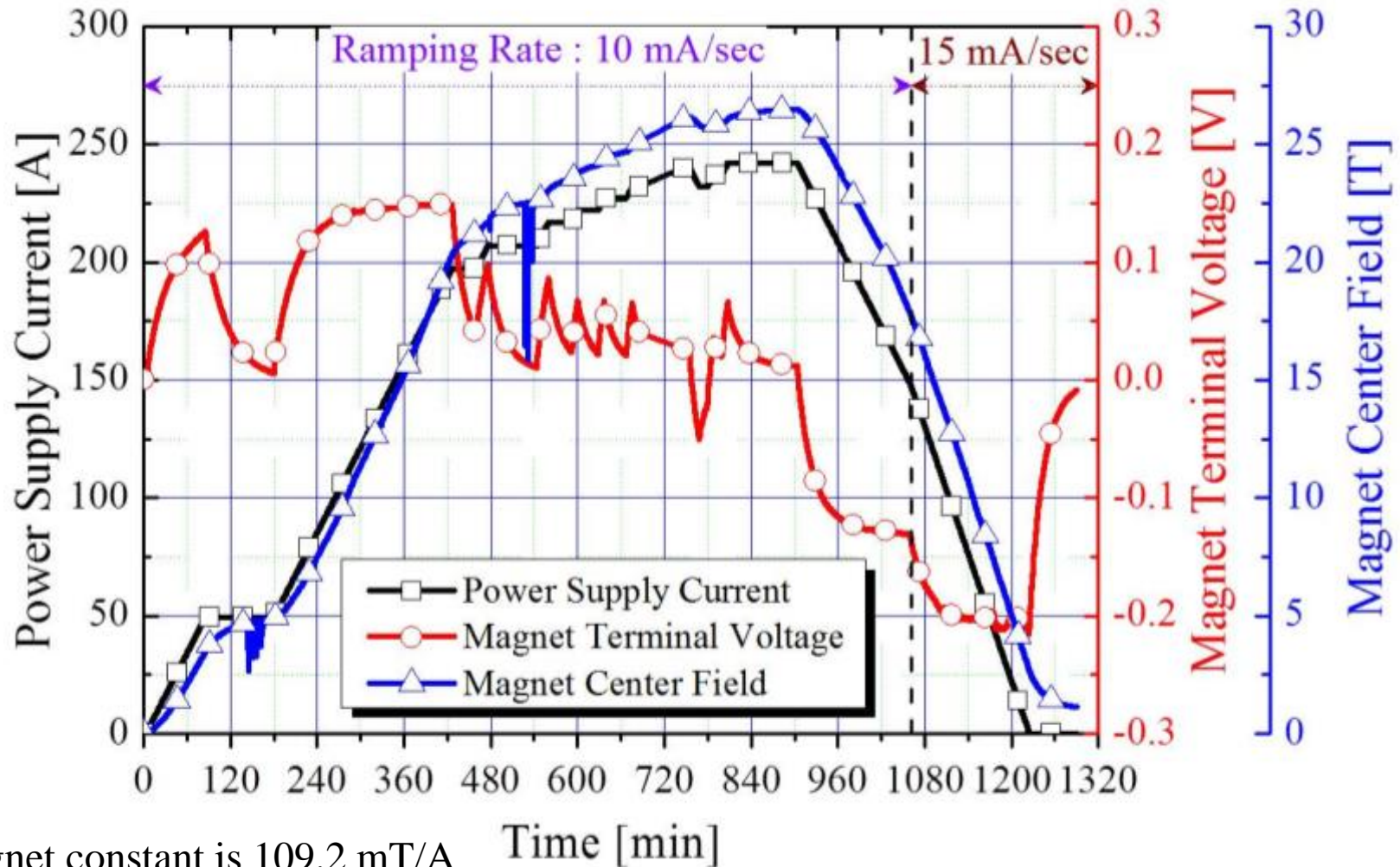
Magnet Assemble

- ✓ completed magnet after the final assembly in accordance with the stacking order



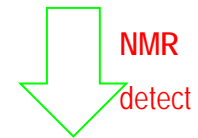
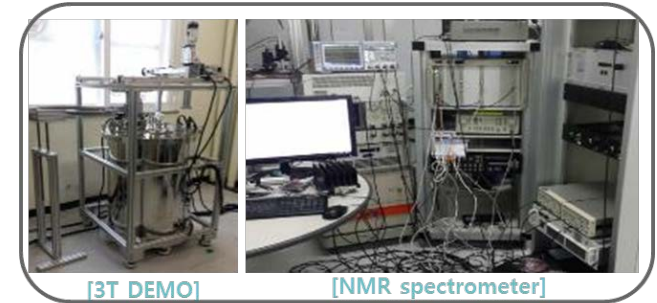
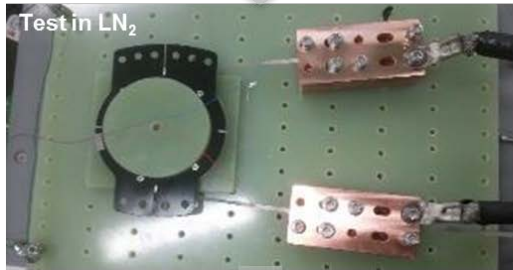
Magnet operation in LHe

- ✓ The magnet center field reached **26.4 T** at 242 A (404 A/mm² for 4.1-mm DPC)

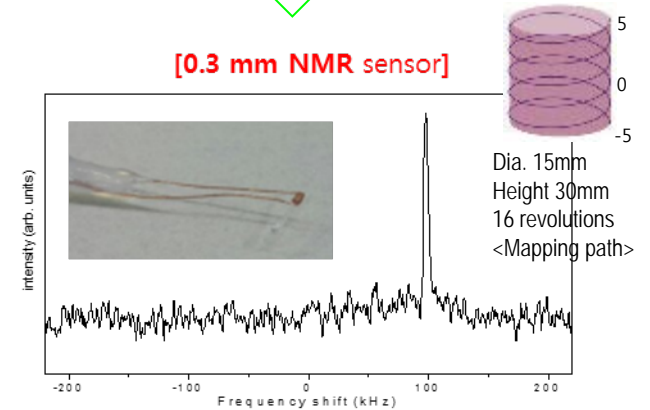


- ✓ Magnet constant is 109.2 mT/A

Cryogen free all HTS NMR



[0.3 mm NMR sensor]



18 T magnet for Axion detection @IBS, Korea

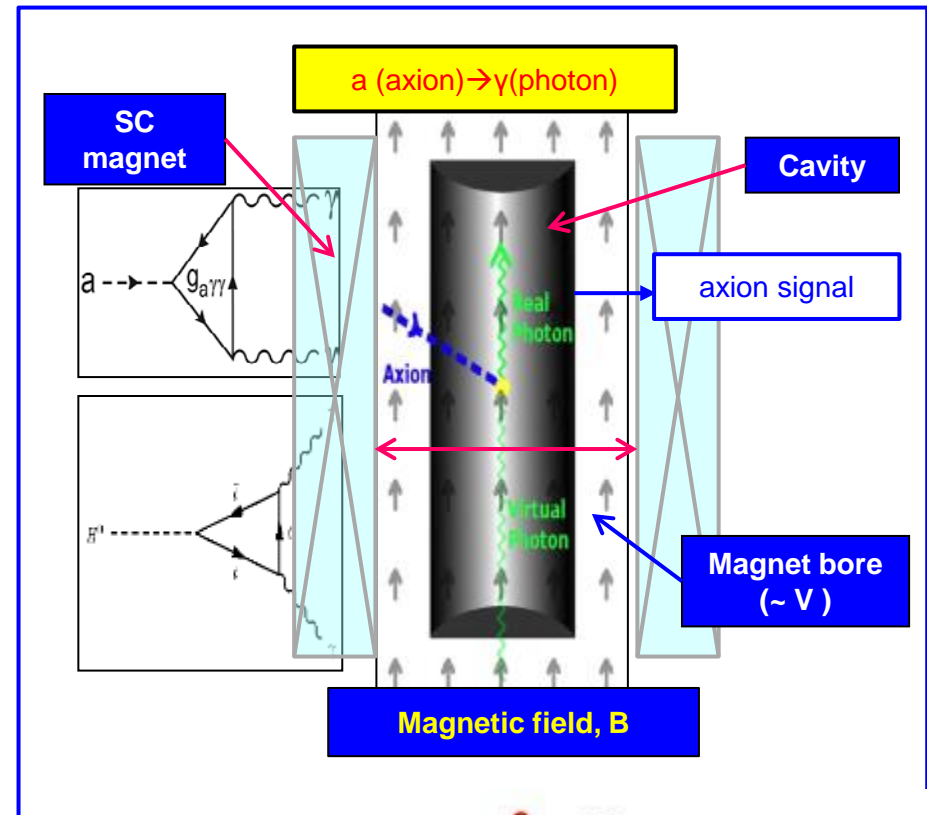
Axion to photon conversion power :

$$P = \underbrace{g_{\alpha\gamma\gamma}^2}_{\text{axion-photon - photon coupling}} \frac{\rho_a}{m_a} \underbrace{V B_0^2}_{\text{Magnetic field \& cavity volume}} \underbrace{C \min(Q_L, Q_a)}_{\text{cavity}}$$

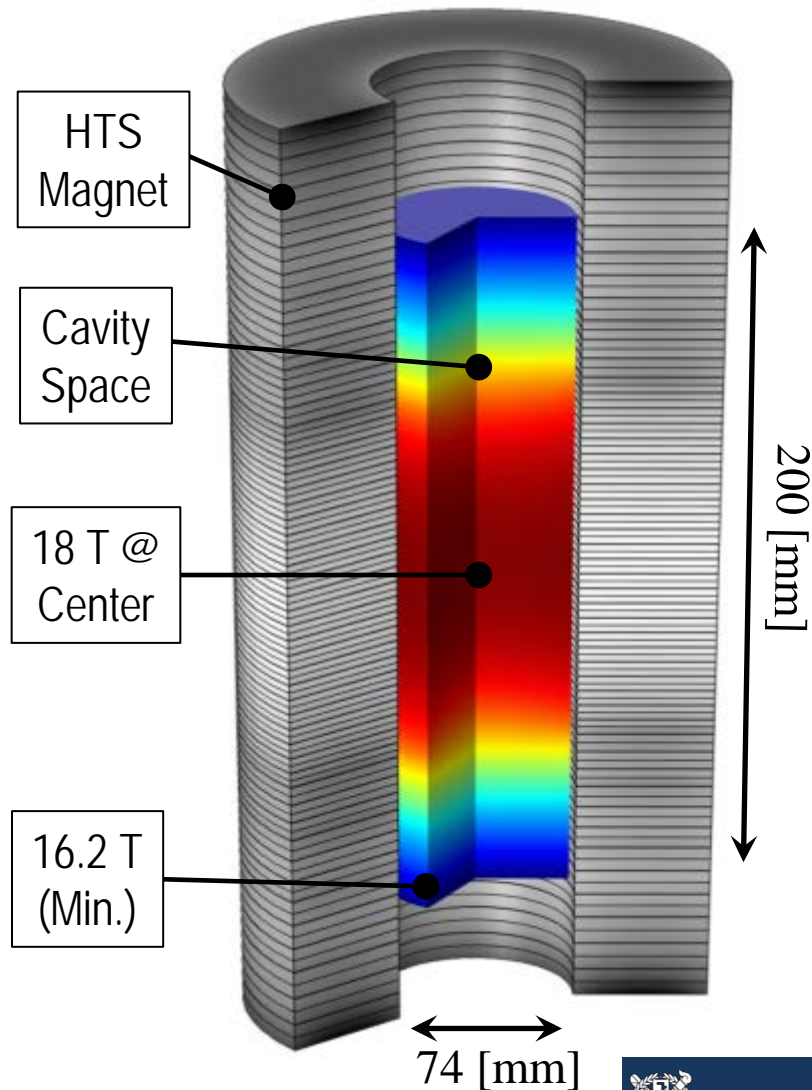
➤ Axion-photon conversion : proportional to $B^2 \cdot V$

⇒ **Strongly Depends on the Magnet**

axion signal power is exceedingly weak, $<10^{-21}$ Watt (zepto-watt)



18 T magnet -design



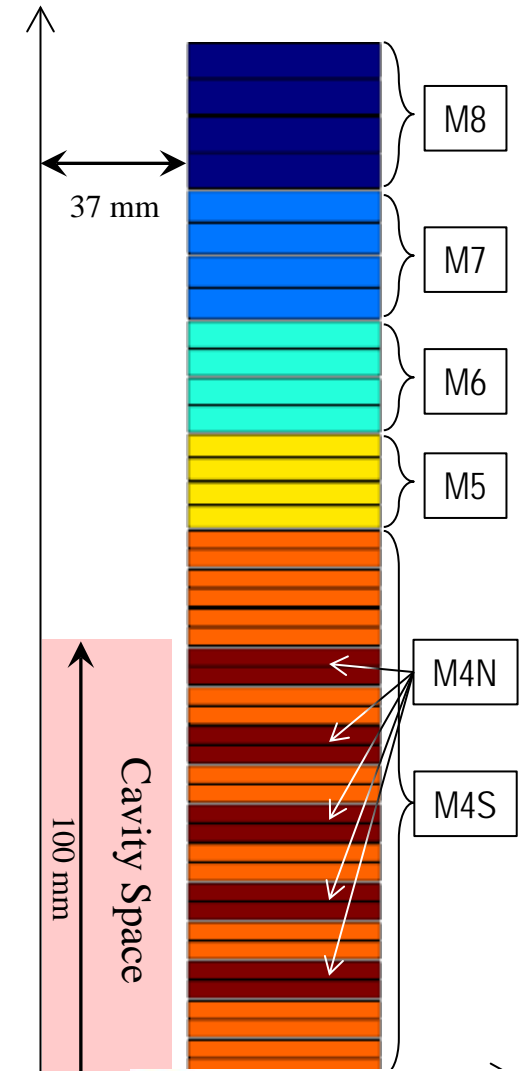
◆ Key design parameters

- 18 T at magnet center
- In 66 mm Φ , 200 mmL cylinder,
90 % Uniformity in Cavity Space
 - $|B| \geq 16.2$ [T]
- Operating in liquid helium (4.2 K)

18 T magnet - design

Coil Configuration	Unit	M4N	M4S	M5	M6	M7	M8
Tape Dimension	[mm]	4.1	4.1	5.1	6.1	7.1	8.1
Tape Thickness	[mm]	0.12	0.14	0.12	0.12	0.12	0.14
Cold Bore; Magnet Height	[mm]	70; 476					
Winding I.D.; O.D.	[mm]	74.0; 162					
Number of DPC		10	18	4	4	4	4
Turn per SPC		365	322	364	363	366	317
Operating Current, I_{op}	[A]	202.6					
Magnetic Field at Center	[T]	18.0					
Min. B in Cavity Space ($z < \pm 100$ mm)	[T]	16.7 (92.5 %)					
Inductance	[H]	20.2					
Stored Energy	[kJ]	375					
Magnetic Hoop Stress	[MPa]	276					
Eng. Current Density	[A/mm ²]	408	358	328	274	236	181
Peak Magnetic Hoop Stress	[MPa]	280 @ M4N(DP20)					

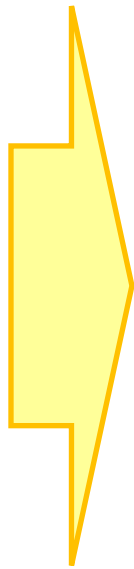
< Upper Half Magnet >



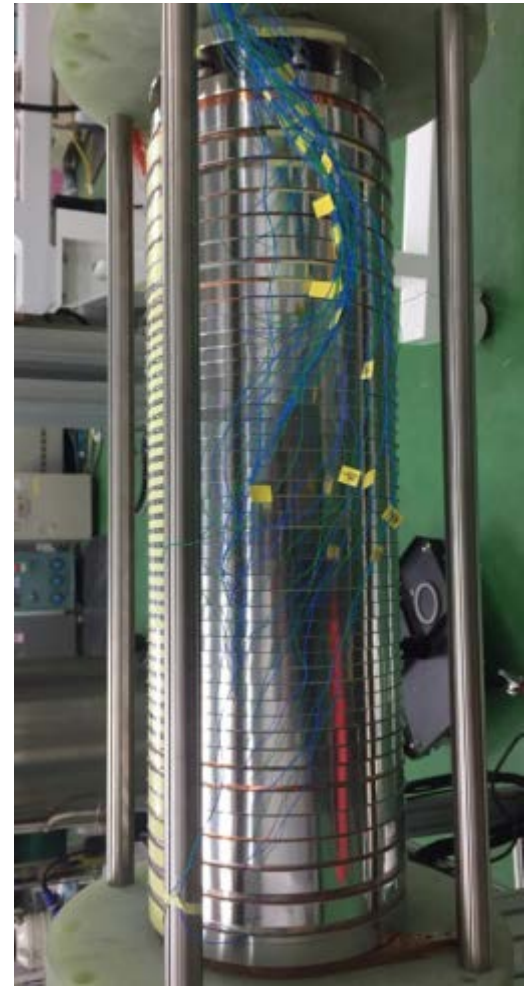
18 T magnet - assemble



< DP Stack >

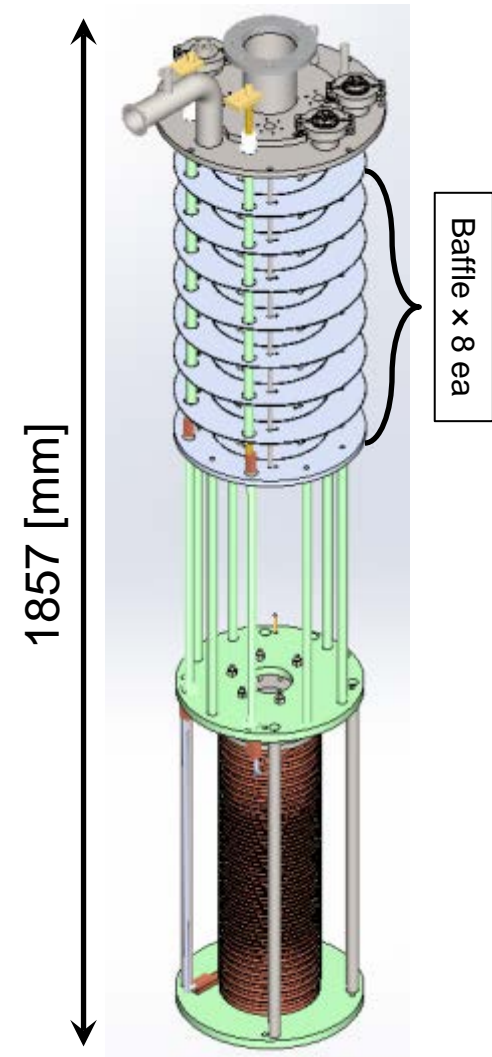
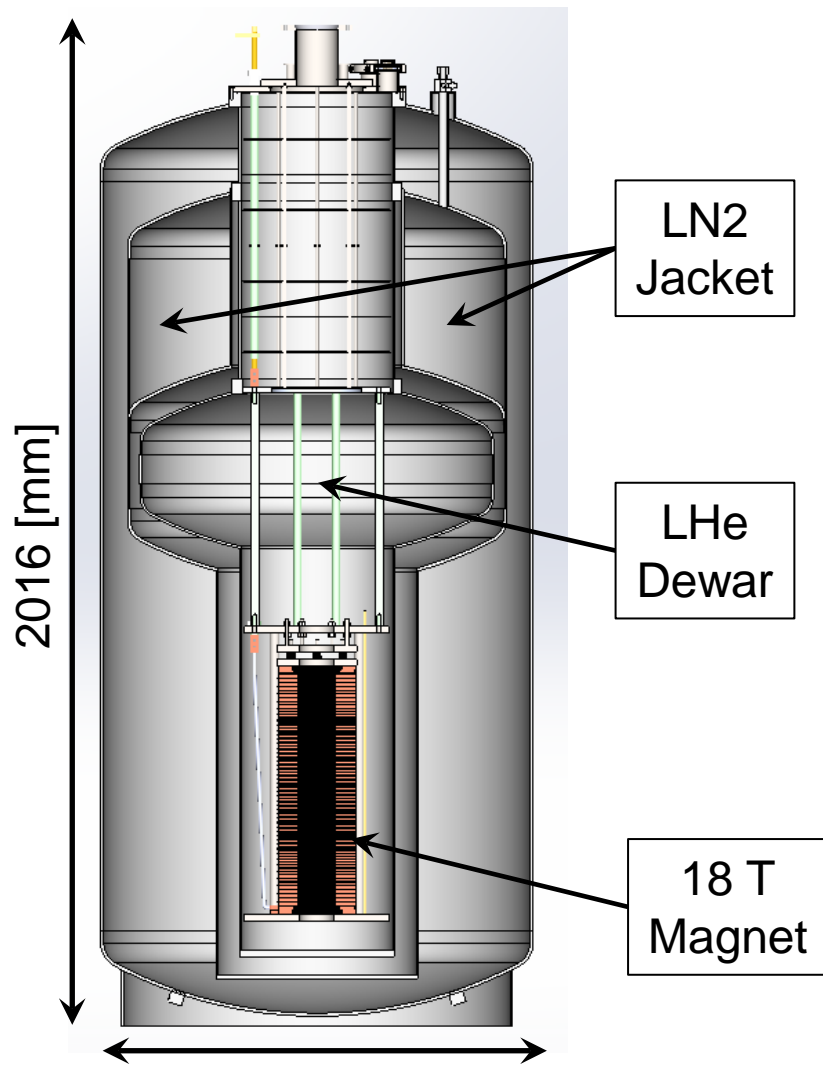


< Splice Joints >

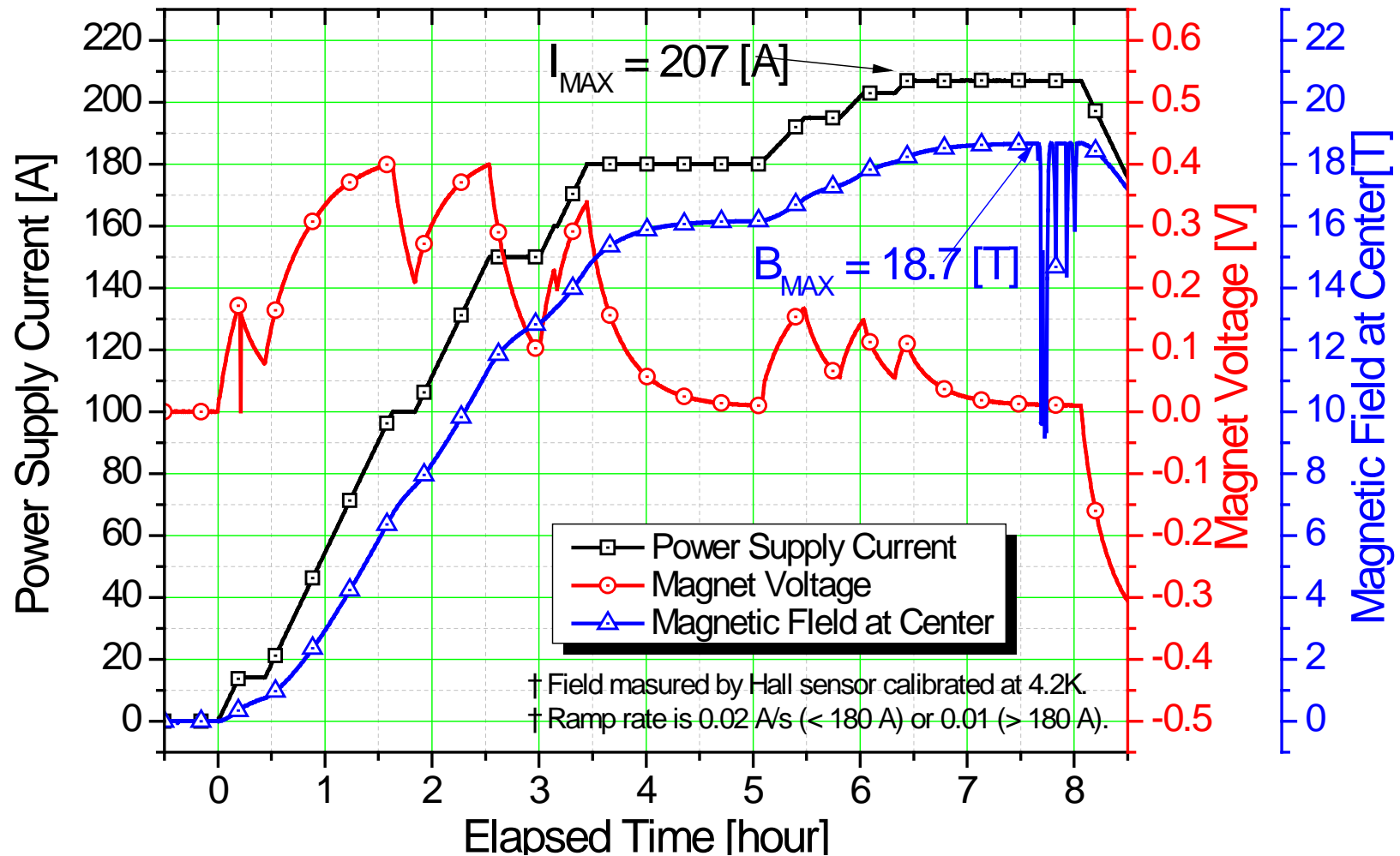


< Overbanding >

18 T magnet - cryostat

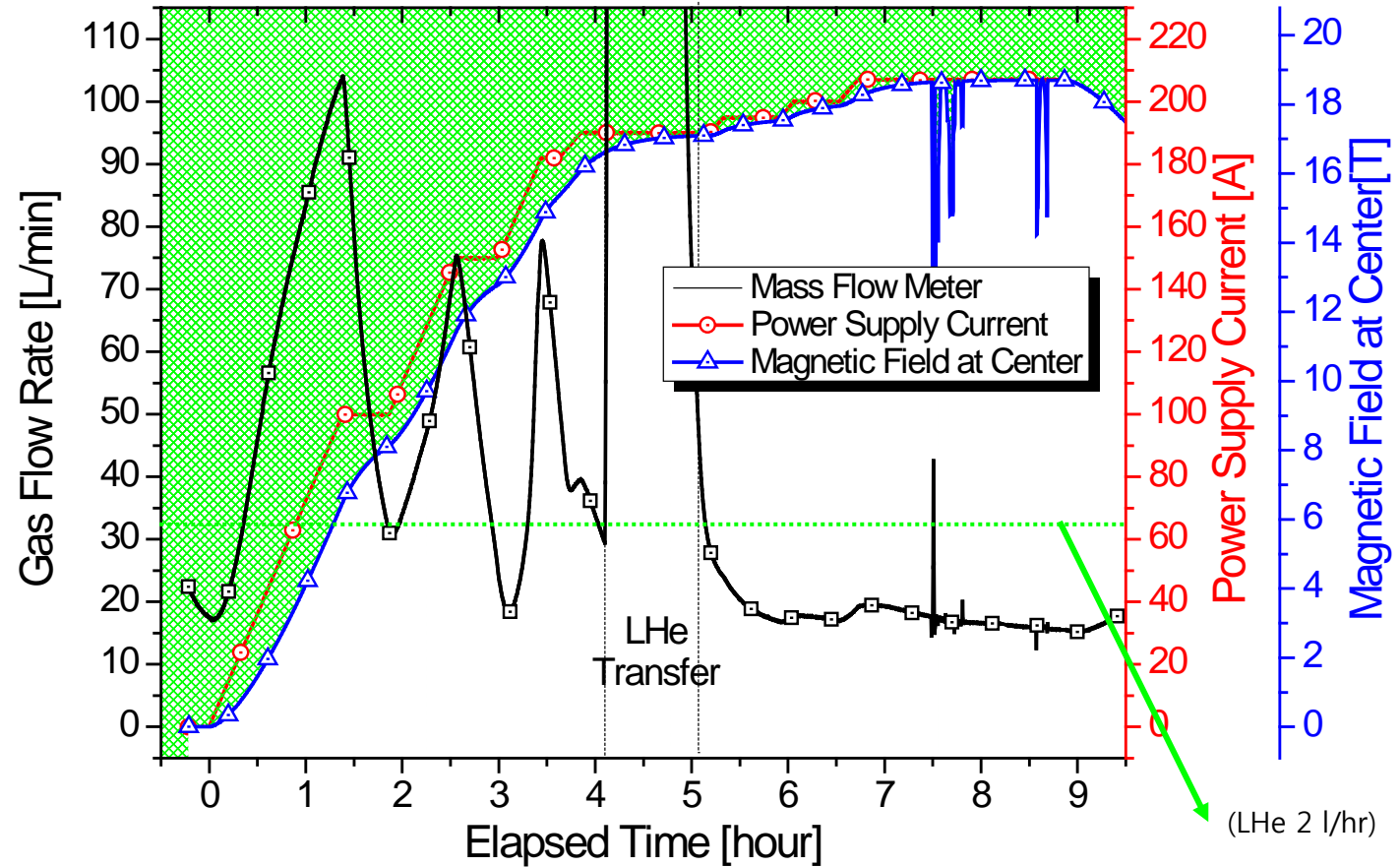


18 T magnet - operation



- Field measured by hall sensor calibrated at 4.2 K
- Ramp rate : 0.02 A/s (under 180 A), 0.01 A/s (Over 180 A)

LHe Consumption @ 18 T



- Temperature of Outlet Gas : 15 ~ 25 °C_s
- Correlation Between Radial Current & Heat

18 T magnet – delivery & comparison to 26 T



✓ Delivered to Center for Axion and Precision Physics Research, IBS(Institute for Basic Science) in Korea; Aug. 2017.

✓ **18.7 T at 4.2 K, 70 mm clear bore.**

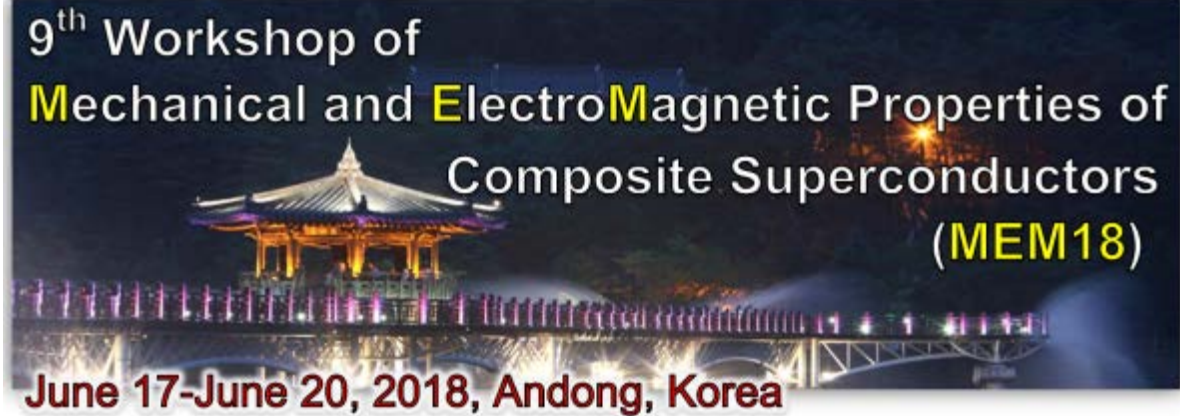
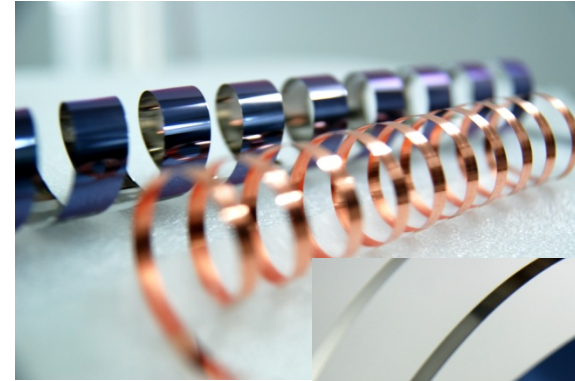
✓ Compared to 26 T magnet twice larger I.D.(2.1X), slightly smaller O.D.(0.9X), ~1.5 times taller, roughly the same stored energy about 20% more tape used

✓ LHe boil rate < 2 liters/hr

Summary

- SuNAM has been producing high I_C coated conductors consistently.
- Introduction of in-line Q.C. measures enhanced wire uniformity & production yield.
- With thicker(1.3 mm \rightarrow 1.6 mm) S.C. layer, we achieved $>1,000$ A/12 mm in production.
- We have made different kinds of NI magnet for various applications.

Thanks for Attention !



<http://mem18.org/>

MEM18

9th Workshop of Mechanical and Electromagnetic Properties of Composite Superconductors
June 17 - 20, 2018, Andong, Korea

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