



An Acoustic Metasurface: From Transmitted Waves Manipulation to Surface Modes Excitation

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Acknowledgements

➤ Collaborators

- Prof. Ying Wu, KAUST
- Prof. Ping Sheng, Dr. Min Yang, Dr. Guancong Ma, HKUST

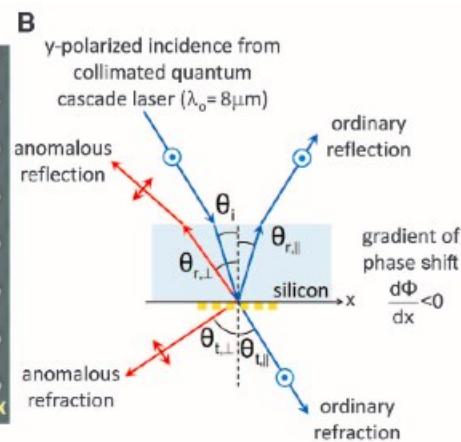
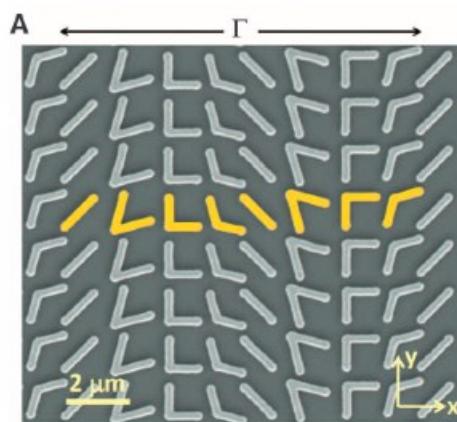
➤ Financial Supports



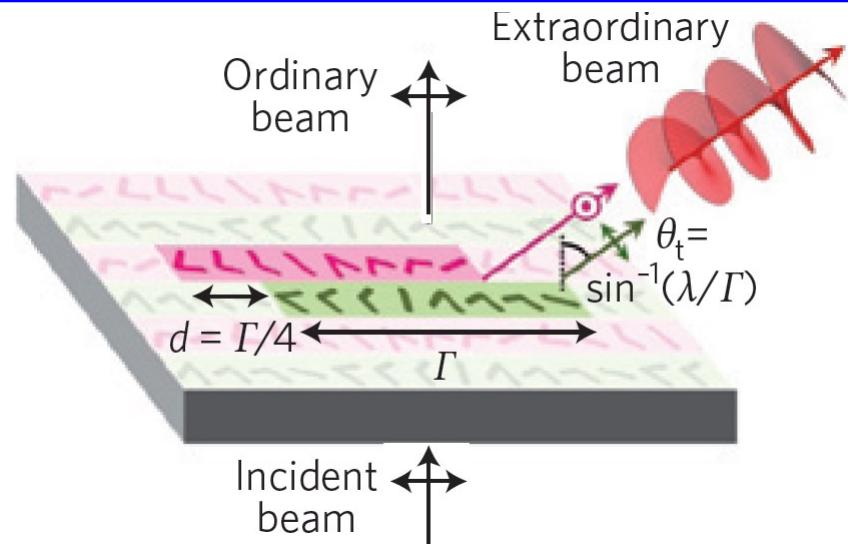
Outline

- Background and motivation
- Our acoustic metasurface
 - Design principle
 - Functionalities
 - A unified analytic model
 - A possible realization
- Summary

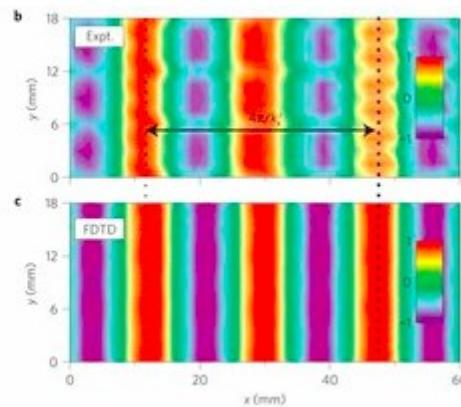
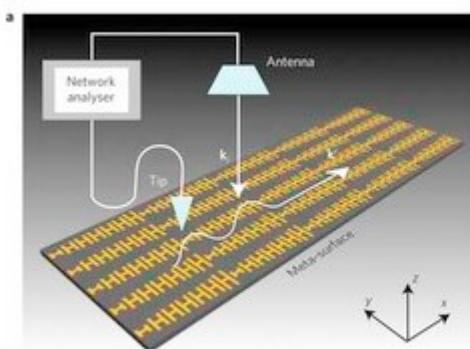
Background: Metasurface for EM waves



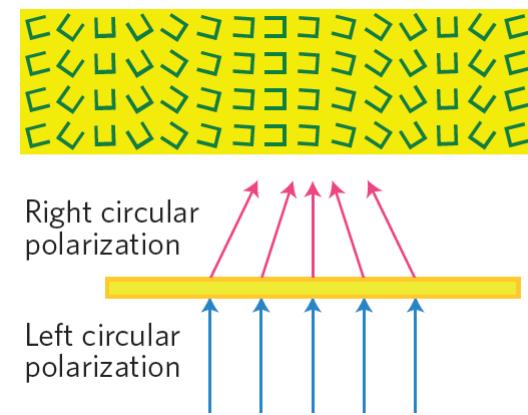
Science 334, 333 (2011)



Nano Lett. 12, 6328 (2012)

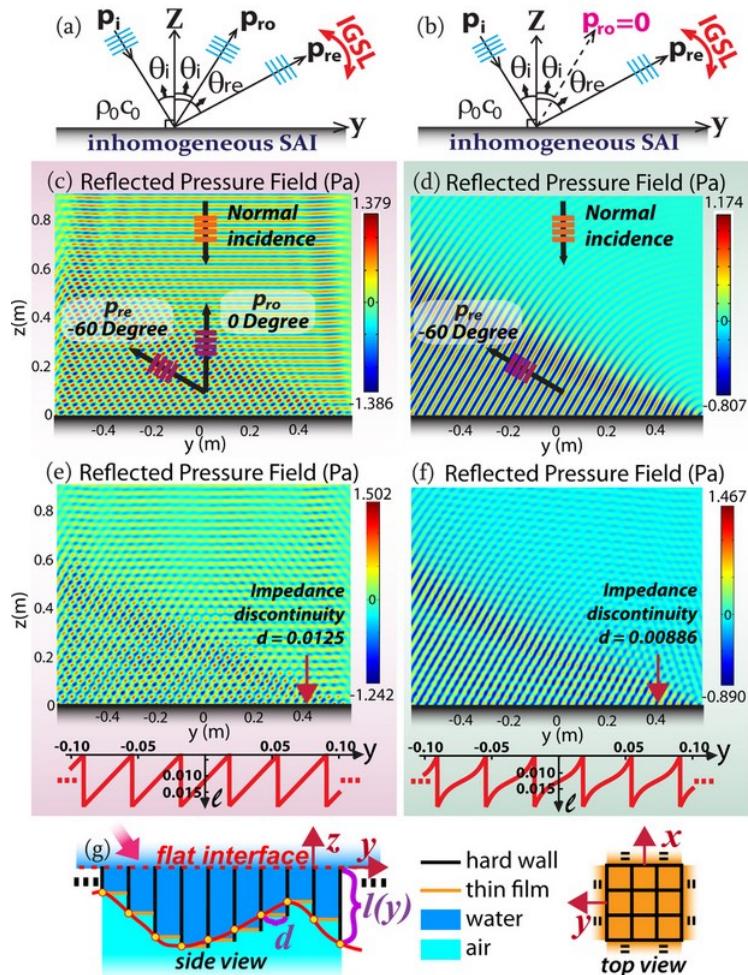


Nat. Mater. 11, 426 (2012)

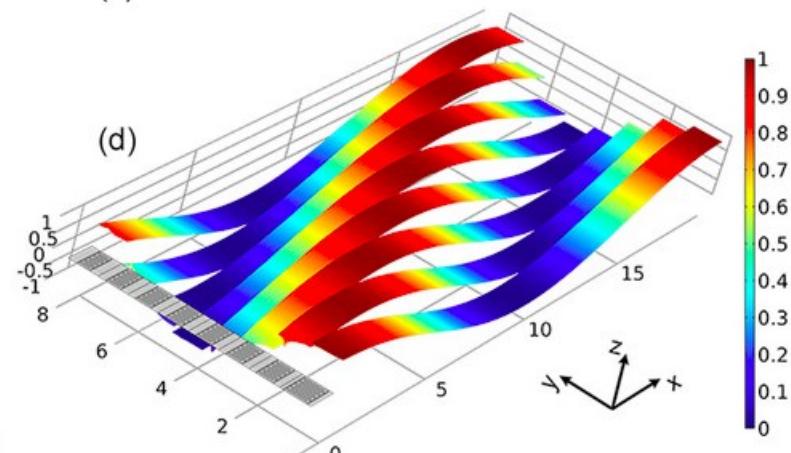


Opt. Express 14, 15882 (2012)

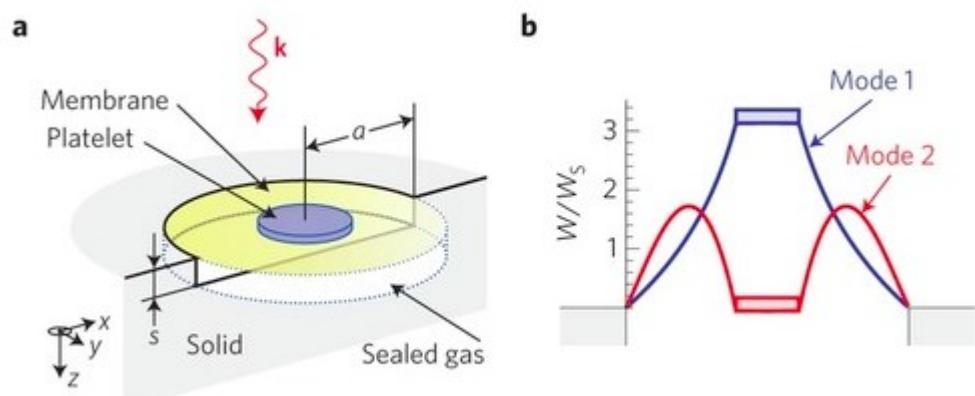
Background: Metasurface for Acoustic Waves



Sci. Rep. 3, 2537 (2013)



Sci. Rep. 3, 2546 (2013)



Nat. Mater. 13, 873 (2014)

Transmitted

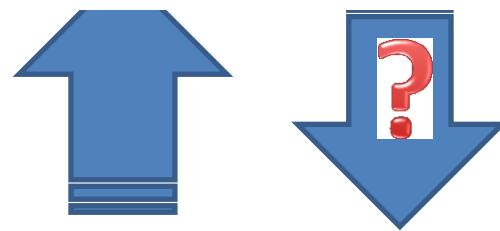


if matched
impedance

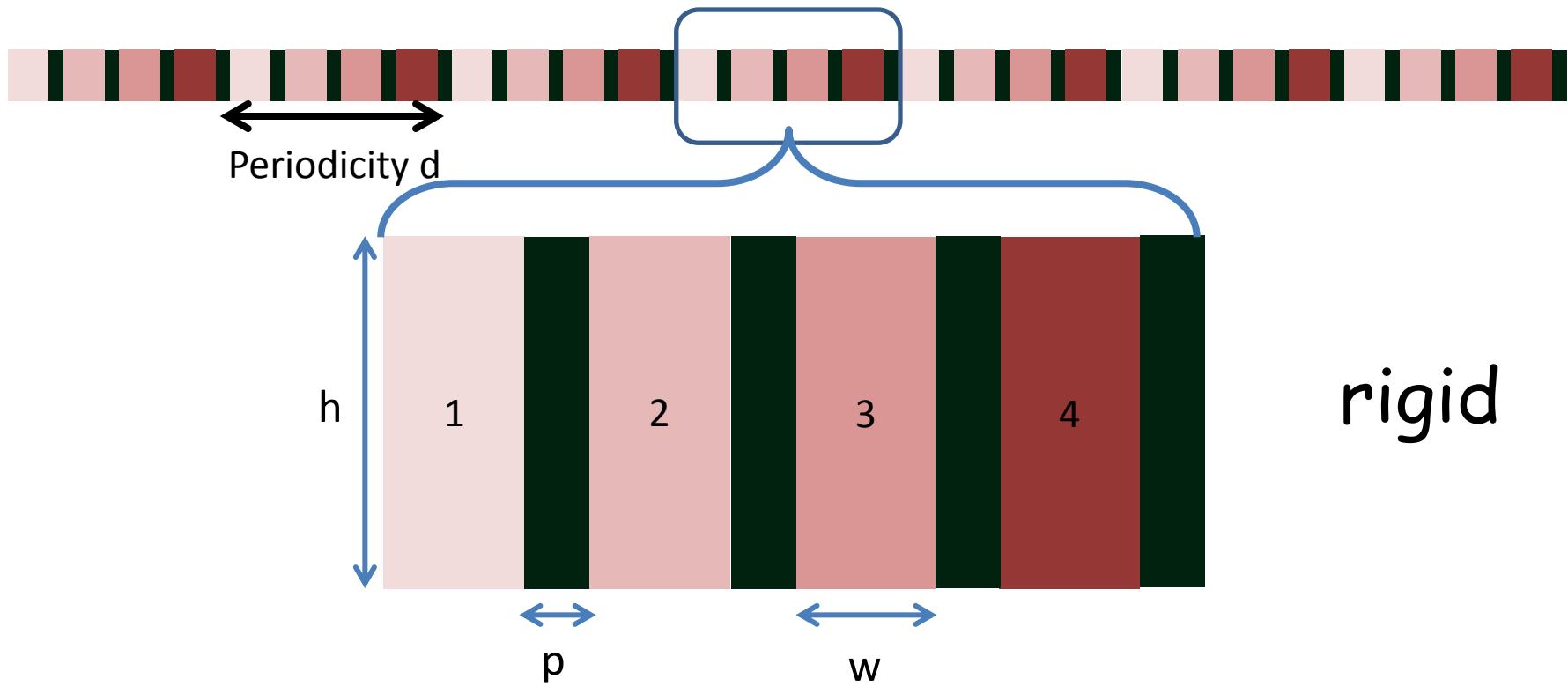


Reflected

Plane wave incidence



Sample design

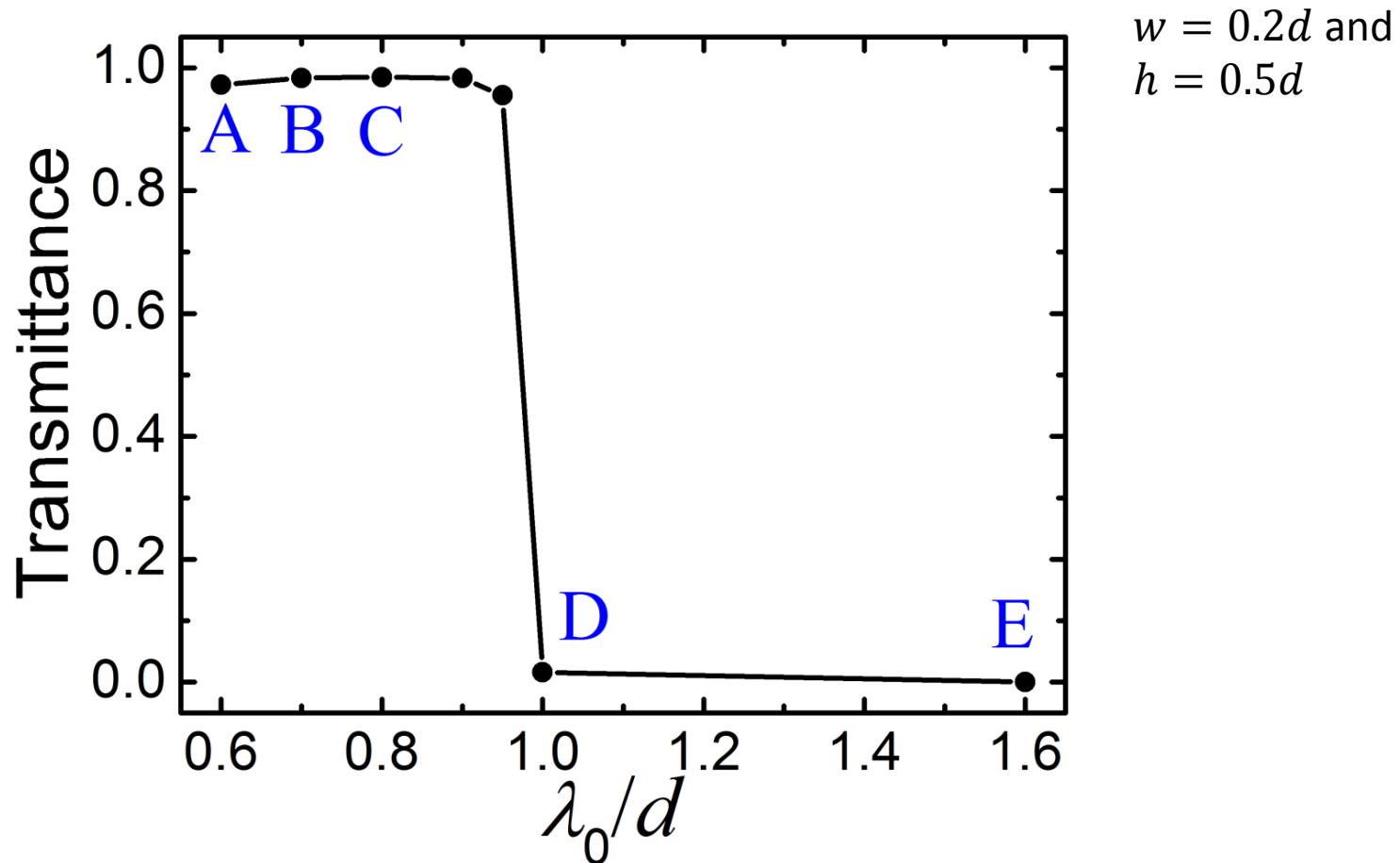


wave velocity: $c_i = c_0 / (1 + (i - 1) \lambda_0 / (mh)) \rightarrow$ Gradient index

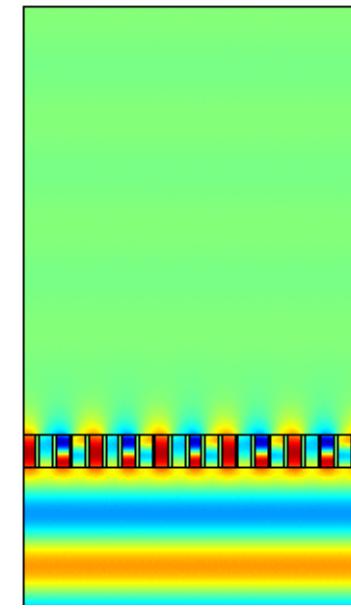
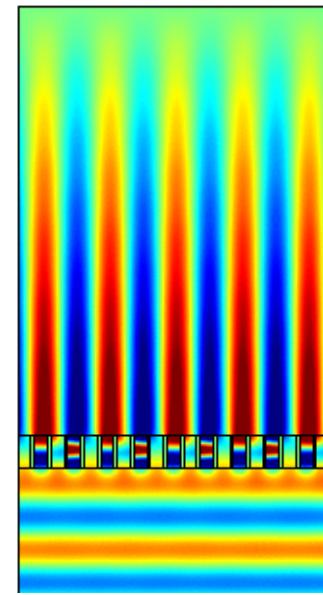
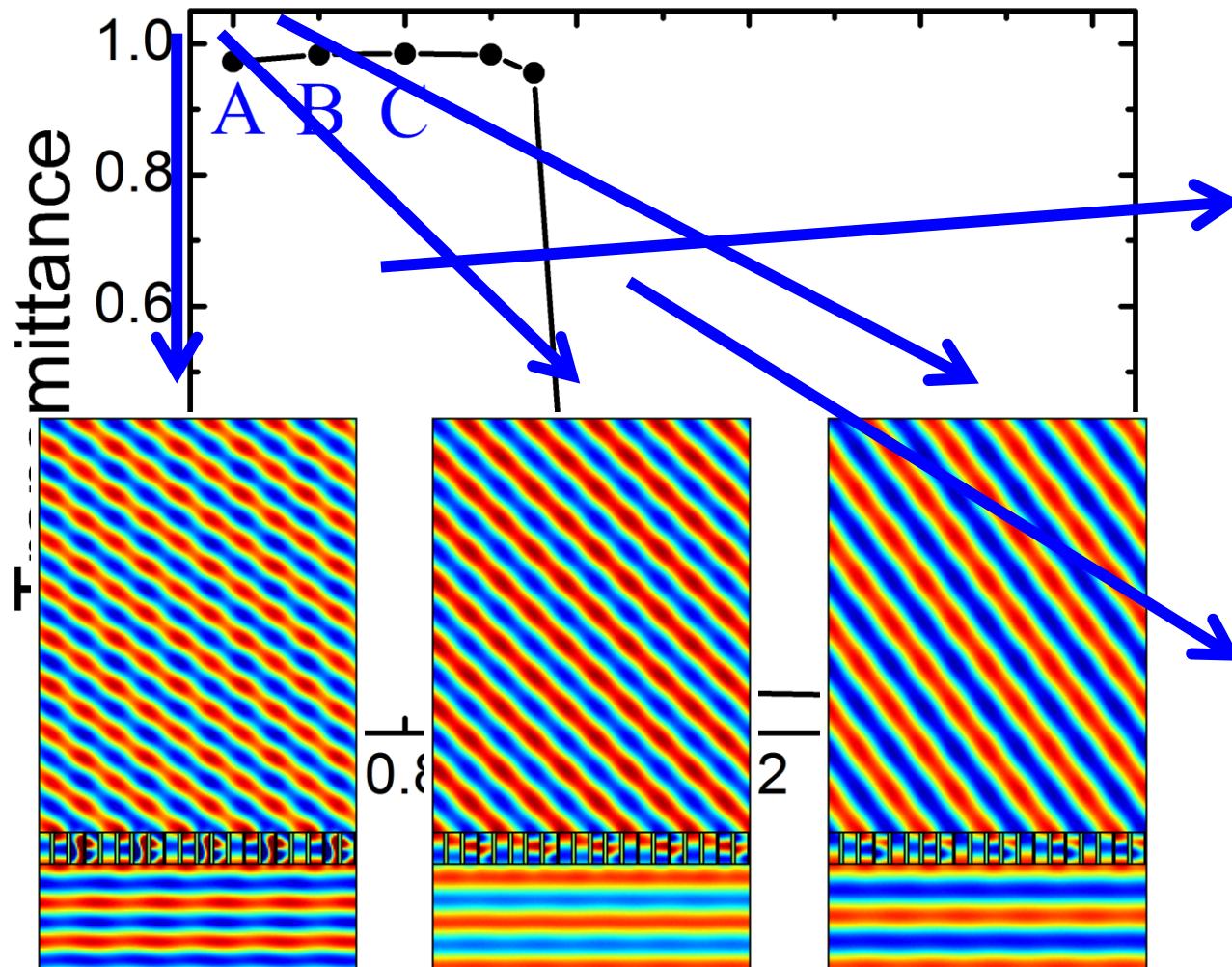
mass density: $\rho_i = \rho_0 (1 + (i - 1) \lambda_0 / (mh))$

Matched-impedance to the background (c_0, ρ_0).

Proof-of-principle demonstration

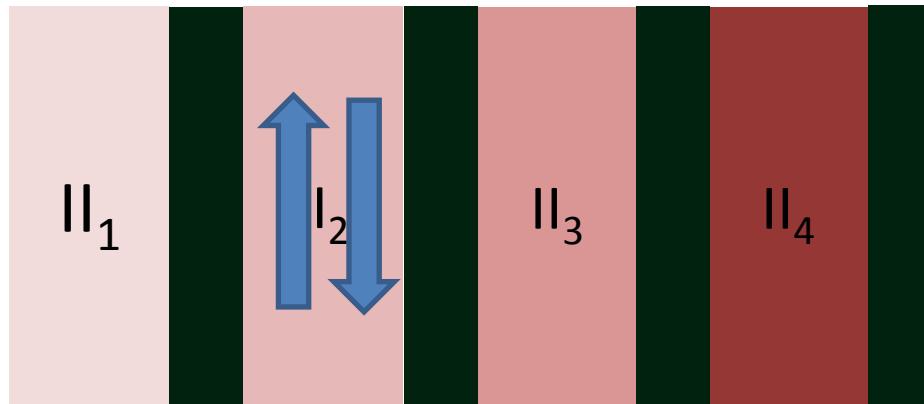


A steep drop of Transmittance from 98% to 1.6% around $\lambda_0 = d$



A unified analytic model based on coupled-mode analysis

Region III: $p^{III} = \sum_i (t_n e^{ik_{y,n} y}) e^{iG_n x}$



$$k_{y,n} = \sqrt{k_0^2 - G_n^2}$$

$$G_n = 2n\pi/d$$

Region I: $p^I = \sum_i (s_{0,n} e^{-ik_{y,n} y}) r_n e^{-ik_{y,n} y} e^{iG_n x}$

Region II: $p^{II} = \sum_i (r_{i,n} e^{ik_{y,n} y}) e^{-ik_{y,n} y}$ (in the i -th slit)

Matching the boundary conditions

$$1 + r_0 + \left(r_1 e^{iG_1 \alpha_i} + r_{-1} e^{iG_{-1} \alpha_i} \right) \operatorname{sinc} \left[\frac{G_1 w}{2} \right] = a_i + b_i \quad (i = 1, 2, 3, 4),$$

$$t_0 + \left(t_1 e^{iG_1 \alpha_i} + t_{-1} e^{iG_{-1} \alpha_i} \right) \operatorname{sinc} \left[\frac{G_1 w}{2} \right] = a_i e^{ik_i h} + b_i e^{-ik_i h} \quad (i = 1, 2, 3, 4),$$

$$(1 - r_0) \frac{k_0 d}{\rho_0} = \sum_{i=1}^4 \frac{k_i w (a_i - b_i)}{\rho_i},$$

$$t_0 \frac{k_0 d}{\rho_0} = \sum_{i=1}^4 \frac{k_i w (a_i e^{ik_i h} - b_i e^{-ik_i h})}{\rho_i},$$

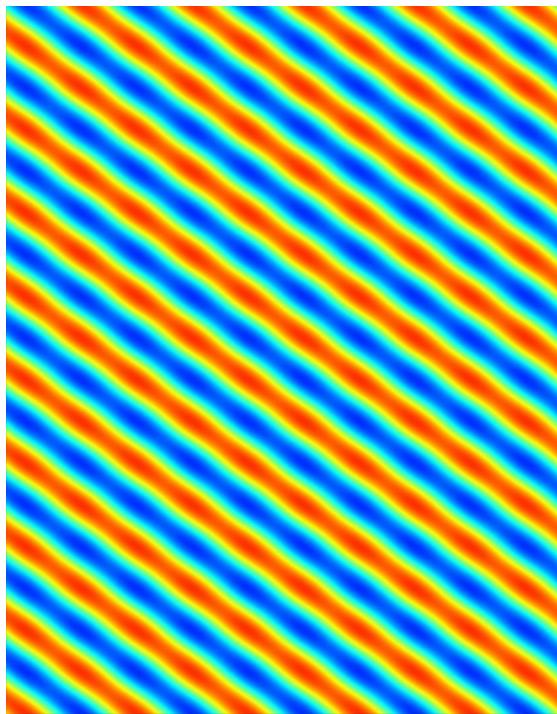
$$-r_{\pm 1} \frac{k_{y, \pm 1} d}{\rho_0} = \sum_{i=1}^4 \frac{k_i w (a_i - b_i) e^{-iG_{\pm 1} \alpha_i}}{\rho_i} \operatorname{sinc} \left[\frac{G_1 w}{2} \right],$$

$$t_{\pm 1} \frac{k_{y, \pm 1} d}{\rho_0} = \sum_{i=1}^4 \frac{k_i w (a_i e^{ik_i h} - b_i e^{-ik_i h}) e^{-iG_{\pm 1} \alpha_i}}{\rho_i} \operatorname{sinc} \left[\frac{G_1 w}{2} \right],$$

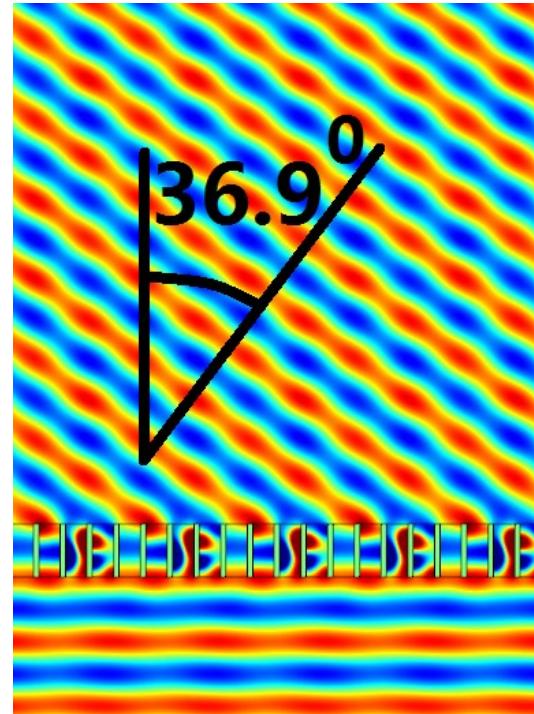
At short wavelength $\lambda_0 = 0.6d$

Analytic model prediction

$$\theta_t = \arcsin(\lambda_0/d) = 36.9^\circ$$



COMSOL Simulation

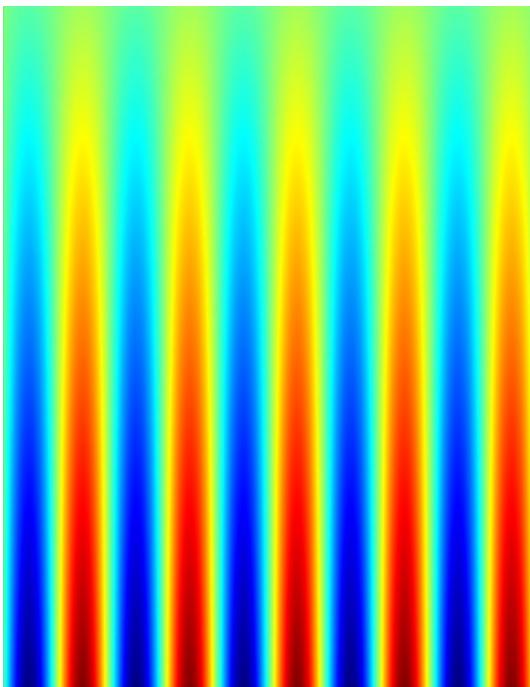


large t_1 , small enough
 t_{-1} and r_0 , while t_0
and $r_{\pm 1}$ are almost 0

At critical point: $\lambda_0 = d$

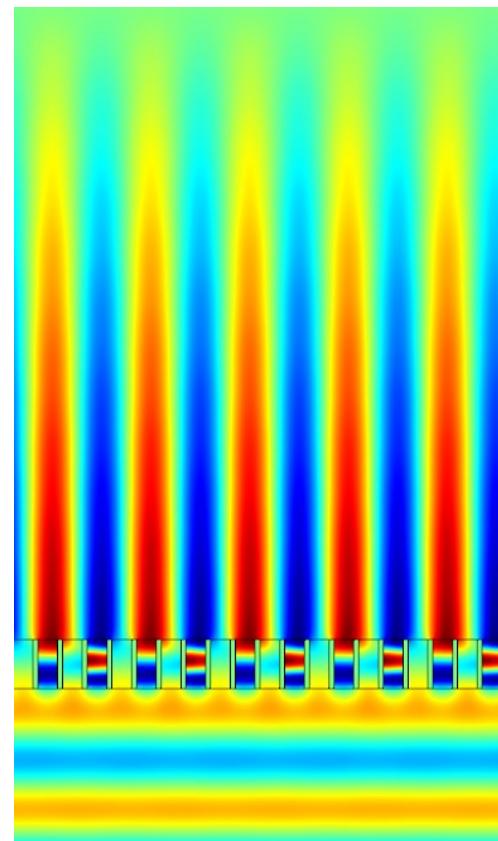
Analytic model prediction

$$k_{y,\pm 1} = \sqrt{k_0^2 - (2\pi/d)^2} = 0$$



large r_0 and $t_{\pm 1}$

COMSOL Simulation



At long wavelength $\lambda_0 = 1.6d$

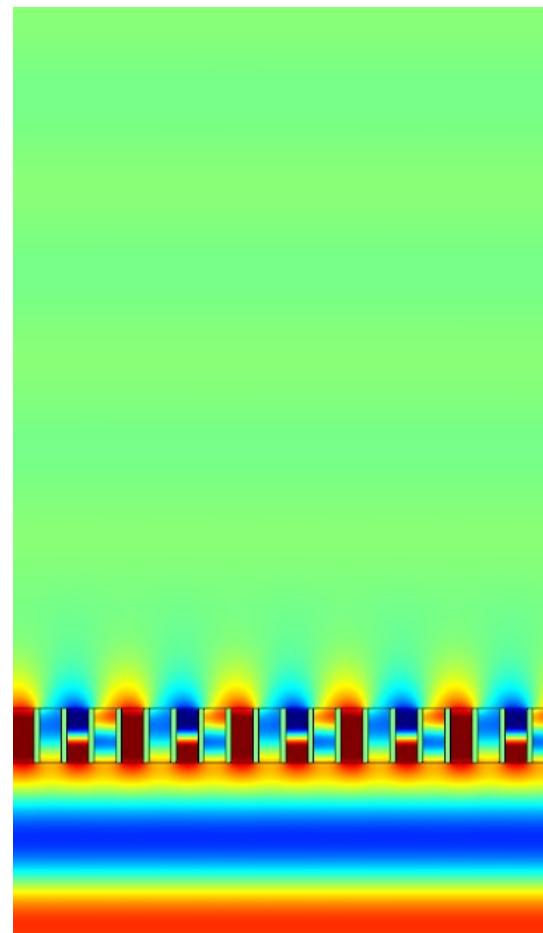
Analytic model prediction

$k_{y,\pm 1}$ are purely **imaginary**



large r_0 and $t_{\pm 1}$, while
 t_0 and $r_{\pm 1}$ are almost 0

COMSOL Simulation



Generalized Snell's law

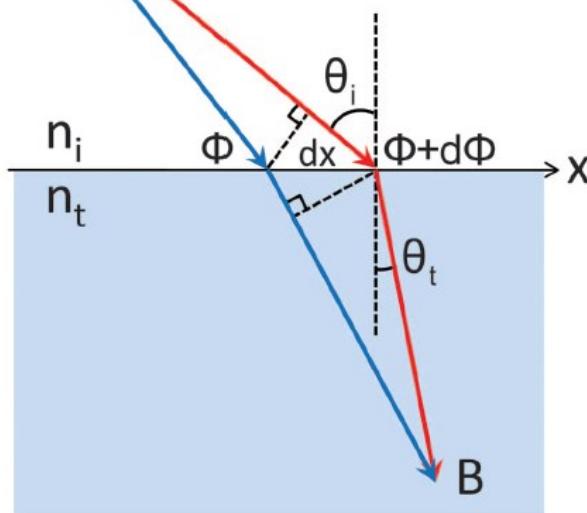
Manipulate wave front by engineering the phase

➤ Fermat's principle:

$$[k_0 n_i \sin(\theta_i) dx + (\Phi + d\Phi)] - [k_0 n_t \sin(\theta_t) dx + \Phi] = 0$$

when $n_t = n_i$, we get

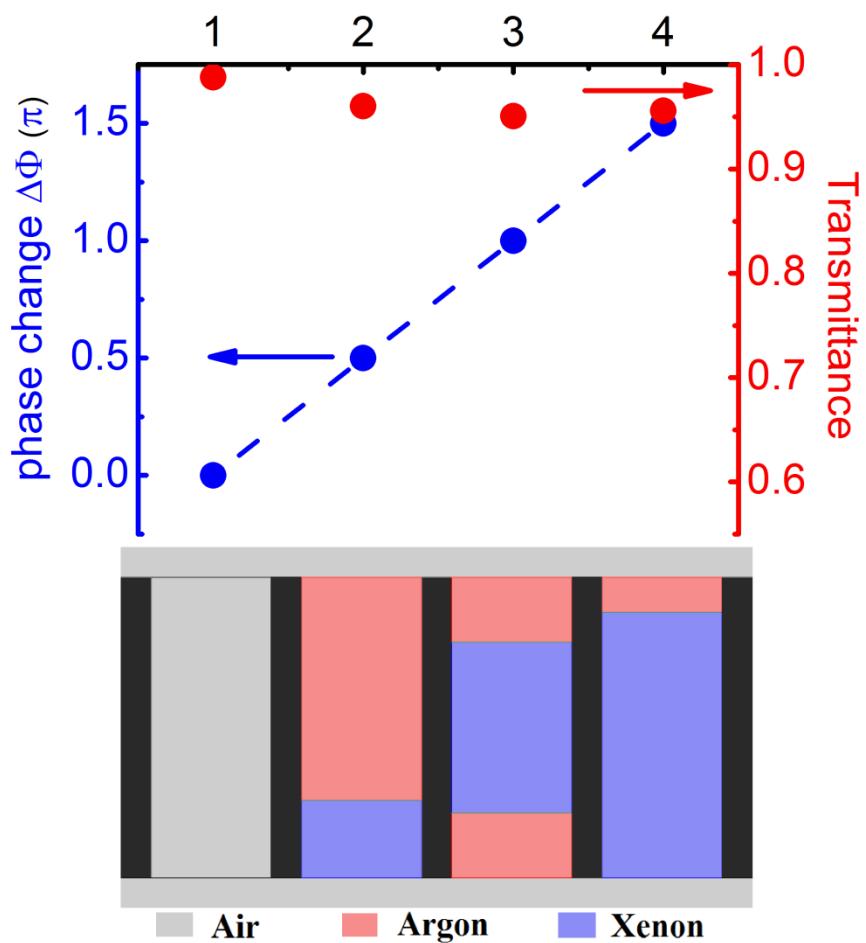
$$k_0 \sin \theta_t - k_0 \sin \theta_i = \frac{d\Phi}{dx}$$



➤ For our metasurface $\frac{d\Phi}{dx} = \frac{2\pi}{d}$

$$\theta_t = \arcsin\left(\frac{\lambda_0}{d}\right)$$

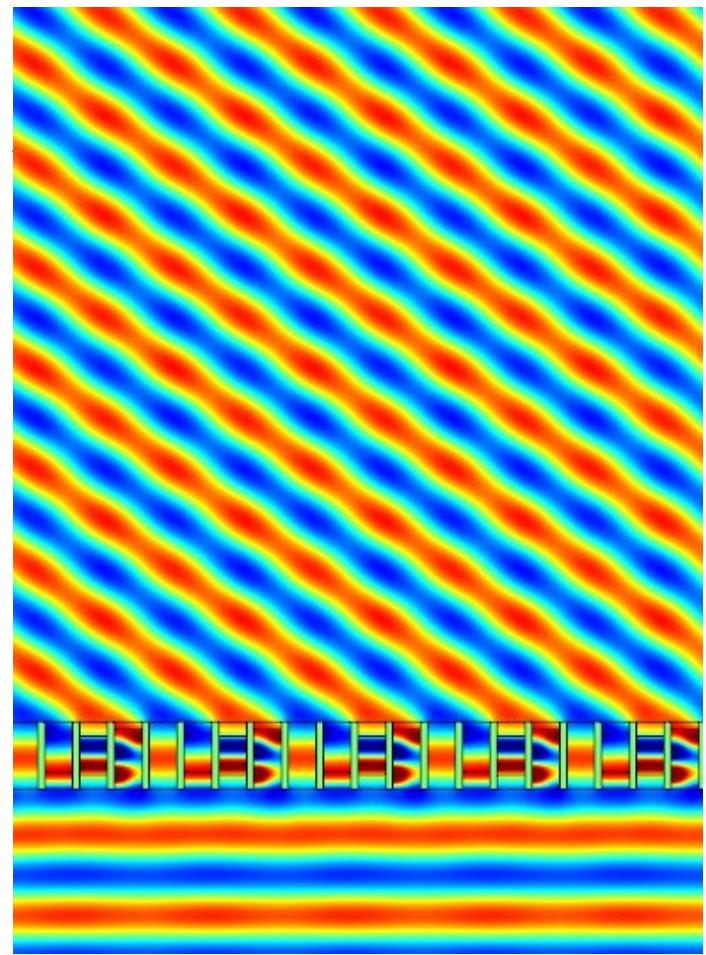
One Realization



$$h_{Arg} + h_{Xen} = h$$

$$\lambda_0 = 0.6d$$

$$\Phi_i = k_{Arg} h_{Arg} + k_{Xen} h_{Xen} = \Phi_1 + (i-1)\pi/2 = k_0 h + (i-1)\pi/2$$



Conclusions

Acoustic metasurface can manipulate acoustic waves

- From normal incidence to oblique transmission or surface bound wave
- Coupled mode theory

Thank you !

